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## TECHNICAL DATA

### Oscillator:

CURVE SHAPE:

Sine-wave

FREQUENCY:

3.15 kHz

Stability:

Approx.  $5 \times 10^{-5}$  within 8 hours

Approx.  $5 \times 10^{-4}$  within 1 year

### OUTPUT:

Voltage (EMF):

Approx. 100 mV<sub>rms</sub>

Impedance:

10 k $\Omega$

### Drift Meter:

RANGE:

$\pm 0.316\%$ ,  $\pm 1\%$ ,  $\pm 3.16\%$  and  $\pm 10\%$

Accuracy:

$\pm 3\%$  of full scale

OFF-SET (calibrated):

0...  $\pm 10\%$

### Wow/Flutter Meter:

RANGE:

$\pm 0.0316\%$ ,  $\pm 0.1\%$ ,  $\pm 0.316\%$ ,  $\pm 1\%$  and  $\pm 3.16\%$

Accuracy:

$\pm 3\%$  of full scale

### Filters:

WOW:

0.2 ... 10 Hz (-3 dB)

FLUTTER:

10 Hz ... 300 Hz (-3 dB)

LIN:

0.2 ... 300 Hz (-3 dB)

WEIGHTED:

Acc. to DIN 45 507, IEC 386, CCIR 409 and IEEE 193

### Meter Circuit:

DIN:

Acc. to DIN 45 507, IEC 386, CCIR 409 and IEEE 193

DIN PEAK:

Acc. to DIN 45 507

Meter reads and automatically retains highest wow/flutter peak value occurring within measuring time of approx. 30 sec.

$\sigma 1$ ,  $\sigma 2$ ,  $\sigma 3$ .

Meter reads and automatically retains highest wow/flutter peak value occurring but excludes random peaks occurring in less than 32% ( $\sigma 1$ ), 4.5% ( $\sigma 2$ ) and 0.26% ( $\sigma 3$ ) of measuring time (5 sec).

### Frequency Analyser:

RANGE:

1 Hz ... 316 Hz in 5 ranges:

1 Hz ... 3.16 Hz, 3.16 Hz ... 10 Hz, 10 Hz ... 31.6 Hz, 31.6 Hz ... 100 Hz

and 100 Hz ... 316 Hz

BANDWIDTH:

10% (-3 dB)

OCTAVE ATTENUATION:

40 dB

LINEARITY:

Frequency:

Better than  $\pm 5\%$

Amplitude:

Better than  $\pm 1$  dB

REMOTE (Option):

Control voltage:

0 ... +10 V in all ranges (linearity better than  $\pm 5\%$ )

Input impedance:

Approx. 10 k $\Omega$

<b>Inputs:</b>	Common to drift, wow and flutter Automatic indication (»NO INPUT«) at too-low input voltage, simultaneously with switching the internal reference oscillator on.
<b>PHONO, LOW-IMPEDANCE:</b>	5-pole DIN
Voltage:	3 mV ... 10 V
Impedance:	47 k $\Omega$ $\pm$ 5%
<b>PHONO, HIGH-IMPEDANCE:</b>	5-pole DIN
Voltage:	30 mV ... 10V
Impedance:	470 k $\Omega$ $\pm$ 5%
<b>TAPE:</b>	5-pole DIN
Voltage:	30 mV ... 10 V
Impedance:	470 k $\Omega$ $\pm$ 5%
<b>Outputs:</b>	
<b>DRIFT:</b>	BNC
Voltage:	$\pm$ 1 V DC $\pm$ 3% at full scale
Impedance:	10 k $\Omega$ $\pm$ 1%
<b>WOW/FLUTTER, AC:</b>	BNC
Voltage:	1 V AC $\pm$ 3% at full scale
Impedance:	10 k $\Omega$ $\pm$ 1%
<b>WOW/FLUTTER, DC:</b>	BNC
Voltage:	1 V DC $\pm$ 3% at full scale
Impedance:	10 k $\Omega$ $\pm$ 1%
<b>Remote (Option):</b>	37-pole multiconnector All functions and ranges remotely controllable (TTL-compatible)
<b>Power Supply:</b>	110/220 VAC $\pm$ 10%, 50 ... 400 Hz
Power consumption:	Approx. 10 W
<b>Temperature Range:</b>	0 ... 50° C
<b>Dimensions:</b>	
Width:	323 mm
Depth:	210 mm
Height:	160 mm
<b>Weight:</b>	5.7 kg (12.6 lbs)
<b>Finish:</b>	Silver grey and blue enamel
<b>Accessory:</b>	1 instruction manual 1 cable, 5-pole DIN/5-pole DIN
<b>Option 1:</b>	Remote control
<b>Option 2:</b>	Crystal oscillator instead of built-in RC oscillator

**Subject to change without notice**

## INTRODUCTION

The B&O Wow/Flutter Meter WM1 is a combination instrument specially designed for use in testing and repairing record players, tape recorders and other recording and playback equipment.

It is essentially composed of:

1. Driftmeter for measurement of speed deviations within the range  $0 \dots \pm 20\%$  in relation to a built-in 3.15 kHz reference oscillator.
2. Wow/flutter meter for measurement of wow (0.2 Hz ... 10 Hz), flutter (10 Hz ... 300 Hz) or wow plus flutter (0.2 Hz ... 300 Hz). Measurement may be carried out linearly, weighted according to DIN 45507, IEC 386, CCIR 409, IEEE 193 or according to a statistical normal distribution (sigma).
3. Spectrum analyser for checking the wow and flutter spectrum within the frequency range 1 ... 316 Hz.

On the back of the instrument are outputs for connections of oscilloscope, ink-recorder, analyser or other type of monitor.

## OPERATION

The Wow/Flutter Meter WM1 is factory prewired for 220 V  $\pm 10\%$  mains voltage but can easily be modified for 110 V  $\pm 10\%$  by wiring the two 110 V primaries of the power transformer in parallel (Fig. 1).

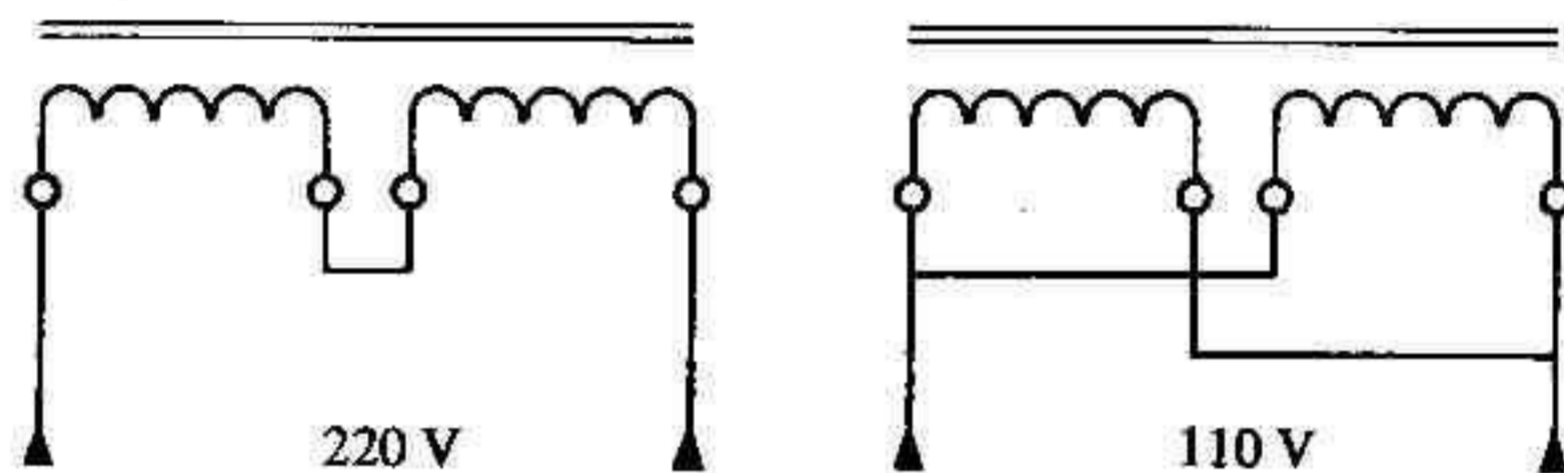


Fig. 1. Modification for 110 V mains voltage.

The mains plug is intended for a special type of outlet with protective earth terminal (*«schuko»*) but may just as well be plugged into a conventional wall outlet although this will cause the cabinet to float.

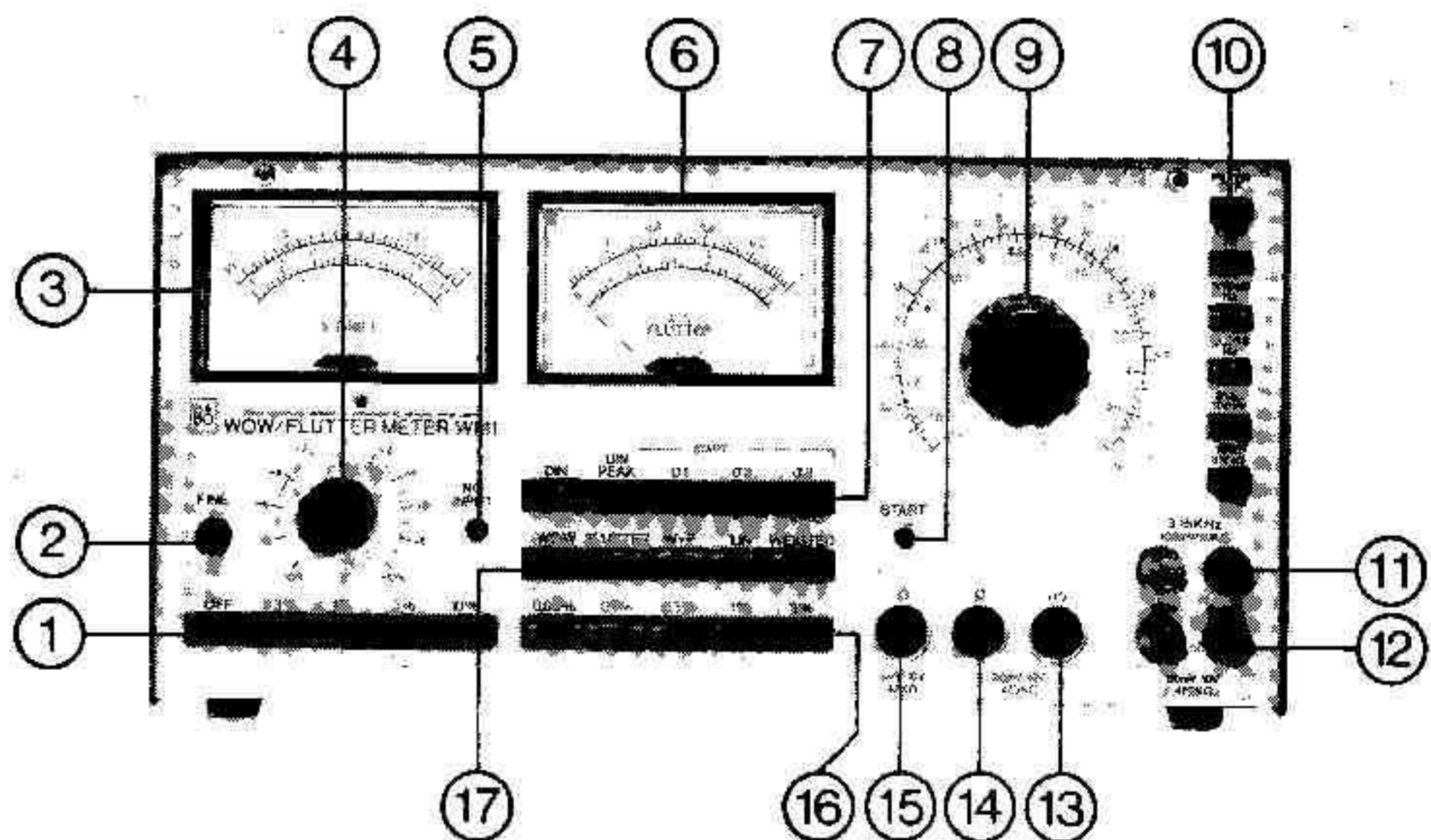


Fig. 2. Front view of Wow/Flutter Meter WM1.

The operation of the instrument appears in broad outline from the following and from Figs. 2 and 3.

1. On/off switch and drift range switch.
2. Drift-offset (speed deviation) fine adjustment. Adjustment range is approx.  $\pm 0.1\%$ .
3. Moving-coil meter for reading drift (speed deviation) in %.
4. Drift-offset (speed deviation) adjustment. Adjustment range is approx.  $\pm 10\%$  (ref. 3.15 kHz).
5. Input voltage indicator. Lamp lights up if input voltage is too low.
6. Moving-coil meter for reading wow and flutter in %.
7. Meter circuit selector.
8. Pushbutton to start measuring cycle with DIN PEAK,  $\sigma 1$ ,  $\sigma 2$ , or  $\sigma 3$  pushbutton depressed.
9. Frequency dial for spectrum analyser.
10. Switch for selecting frequency range of spectrum analyser.
11. Reference oscillator output (3.15 kHz rms).
12. High-impedance connection for record players, tape recorders and other recording/playback equipment not equipped with 5-pole DIN connector.
13. High-impedance DIN connector for tape recorders and other recording/playback equipment.
14. High-impedance DIN connection for record players with built-in RIAA amplifier.
15. Low-impedance DIN connection for record players without built-in RIAA amplifier.
16. Wow and flutter range selector.
17. Switch for selecting filter characteristic for wow and flutter and switch for selecting linear or weighted filter characteristic.

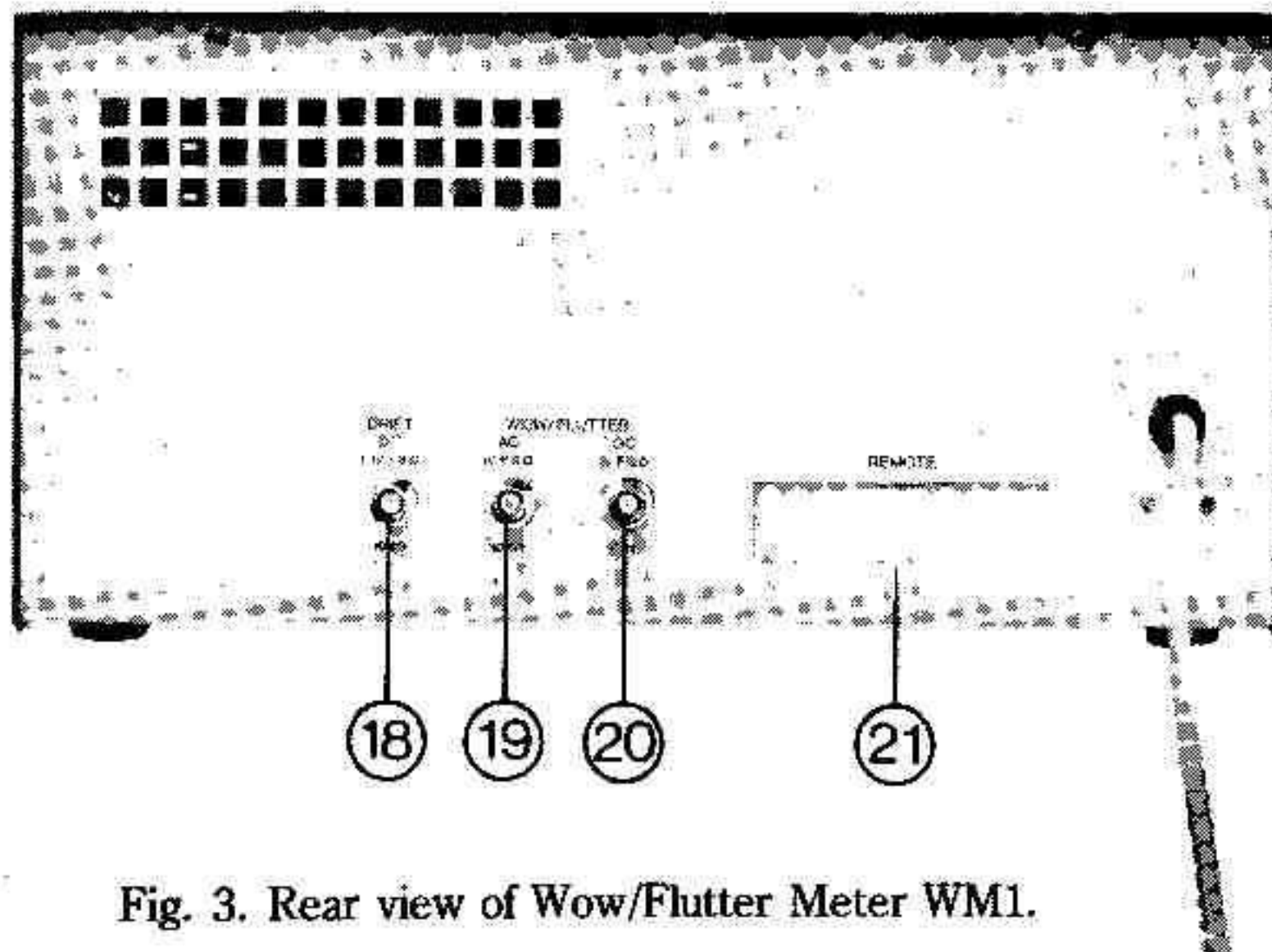


Fig. 3. Rear view of Wow/Flutter Meter WM1.

18. Analog meter output drift (speed deviation). Output voltage is proportional to deflection of DRIFT meter ( $\pm 1$  V at full scale).

19. Analog AC output for wow and flutter. Output voltage is proportional to deflection of FLUTTER meter (1 V at full scale).
20. Analog DC output for wow and flutter. Output voltage is proportional to deflection of FLUTTER meter (1 V at full scale).
21. Remote control (option). All functions and ranges can be remotely controlled through a 37-pole multiconnector (TTL compatible).

### Preparing for Use

The instrument is switched on by depressing one of the drift range buttons (1). The NO INPUT indicator lamp (5) will then light up. Also, the internal reference oscillator is automatically connected to the input, enabling easy zeroing of the DRIFT meter (3) by means of the FINE potentiometer (2) and, if necessary, the DRIFT-OFFSET potentiometer (4). However, such adjustment should not be carried out until after the instrument has had power applied to it for approx. 15 min.

### Connection

The instrument under measurement (record player, tape recorder etc.) is connected to one of the three DIN inputs. Record players without built-in RIAA preamplifier are connected to the  $\phi$  47 k $\Omega$  input (15). Record players with built-in RIAA preamplifier are connected to the  $\phi$  470 k $\Omega$  input (14). Tape recorders are connected to the  $\phi\phi$  input (13). If the instrument under measurement has no provision for DIN connection, the input provided with terminal screws (12) should be used. The built-in reference oscillator is wired to pins 1 and 4, the  $\phi\phi$  input (13) and to the 3.15 kHz terminals (11).

### Measurement of Drift (Speed Deviation) on Record Players

A test record according to DIN 45545, such as a B&O 3621016, should be used as reference. The record player is connected to one of the  $\phi$  inputs (14) or (15). The NO INPUT indicator lamp (5) will then turn off if the input signal is large enough. If it is not large enough it will be necessary to connect the record player through a preamplifier.

The desired range is selected with the pushbutton switch (1), and absolute drift (speed deviation) can then be read on the DRIFT meter (3).

The relative (short-term) speed deviation can be measured all the way down into the most sensitive range (0.3%) by correcting the zero adjustment with the DRIFT OFFSET potentiometer (4) provided the absolute speed deviation is less than  $\pm 10\%$ .

### Measurement of Drift (Speed Deviation) on Tape Recorders

A prerecorded 3150 Hz test tape, such as a B&O 6780037, should be used as reference. The record player is connected to the  $\phi\phi$  input (13) or (12).

The same measuring procedure as for record players.

### Measurement of Wow and Flutter on Record Players

A test record according to DIN 45545, such as a B&O 3621016, should be used as reference.

The desired range is selected with the pushbutton switch (16). The filter function switch (17) is set to the W+F (wow + flutter) and WEIGHTED positions. The meter circuit switch (7) is set to the DIN position.

The analyser range switch (10) is set to the FILTER OFF position.

The weighted wow and flutter can then be read on the FLUTTER meter (6). Measurement should be carried out for not less than 30 sec. Within this period the maximum deflection should be read.

The meter deflection often fluctuates and therefore is difficult to read correctly. The WM1 therefore incorporates a special circuit which is capable of automatically retaining the maximum deflection within the above-mentioned measuring time of 30 sec. The automatic circuit is cut in by setting the meter circuit

switch (7) to DIN PEAK instead of DIN and depressing the START pushbutton (8). After approx. 30 sec the FLUTTER meter will deflect to the maximum value which occurred during the measuring period. The meter needle will remain at that value (for several minutes). When another measuring period is started, the needle returns to zero.

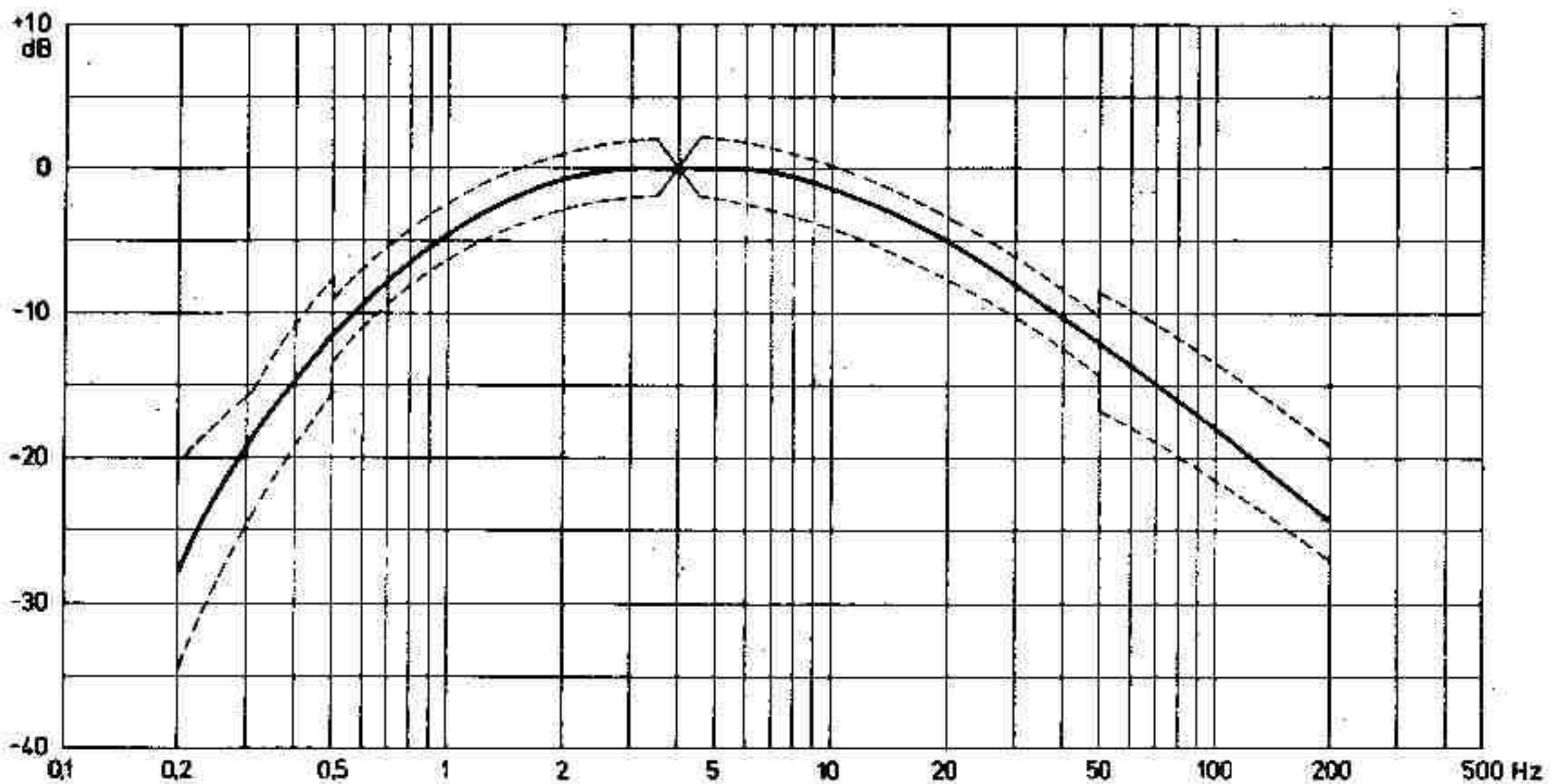


Fig. 4. Wow and flutter filter weighted (WTD).

Accordingly, the results of a DIN and a DIN PEAK measurement are basically the same for one and the same record player.

Because of the WM1's low lower limiting frequency it takes approx. 3 sec for the FLUTTER meter to come to rest after function and range switching. The START button therefore should not be depressed until 3 sec after each switching operation.

#### Measurement of Record/Playback Wow and Flutter on Tape Recorders

A standard tape according to DIN 45513, such as a B&O 6780043 ( $\text{Fe}_2\text{O}_3$ ) or 6780040 ( $\text{CrO}_2$ ), is inserted in the tape recorder whereafter a 3150 Hz signal is recorded at a recording level of  $\text{VU} = 0 \text{ dB}$ . The generator incorporated in the WM1 is employed for this purpose. The signal from it is automatically applied to the tape recorder via pins 1 and 4 of the  $\text{OO}$  input (13) or, as the case may be, the 3.15 kHz terminal screws (11). Recording is carried out for approx. 2 - 3 min., followed by switching to playback. The weighted wow and flutter can now be read on the FLUTTER meter (6), following the directions given under tape recorders.

#### Measurement of Playback Wow and Flutter on Tape Recorders

A prerecorded 3150 Hz test tape is used as reference, e.g. a B&O 6780037. The weighted wow and flutter may then be read on the FLUTTER meter (6), following the directions given under record/playback measurement.

Measurement of playback wow and flutter should not be employed when laying down specifications but is perfectly acceptable in frequency analysis of the wow and flutter spectrum.

#### Measurement of Wow and Flutter on Record Players and Tape Recorders, Corrected According to a Statistic Normal Distribution

In measurements of wow and flutter according to DIN 45507, IEC 386, CCIR 409 and IEEE 193, the FLUTTER meter deflection, as previously mentioned, often is very irregular. This is because the signal is composed of varying frequencies of more or less constant amplitude, noise pulses, mains-voltage

transients etc. Also, the instrument under measurement is often affected mechanically by small jolts and vibrations from the environment. It can therefore seem a little »unjust« if the result of the measurement is too adversely affected by once-only phenomena basically unrelated to wow and flutter on the instrument under measurement.

To remedy this, the WM1 incorporates a special meter circuit which more or less excludes these once-only phenomena in regard to a statistic normal distribution so that measurements become more uniform.

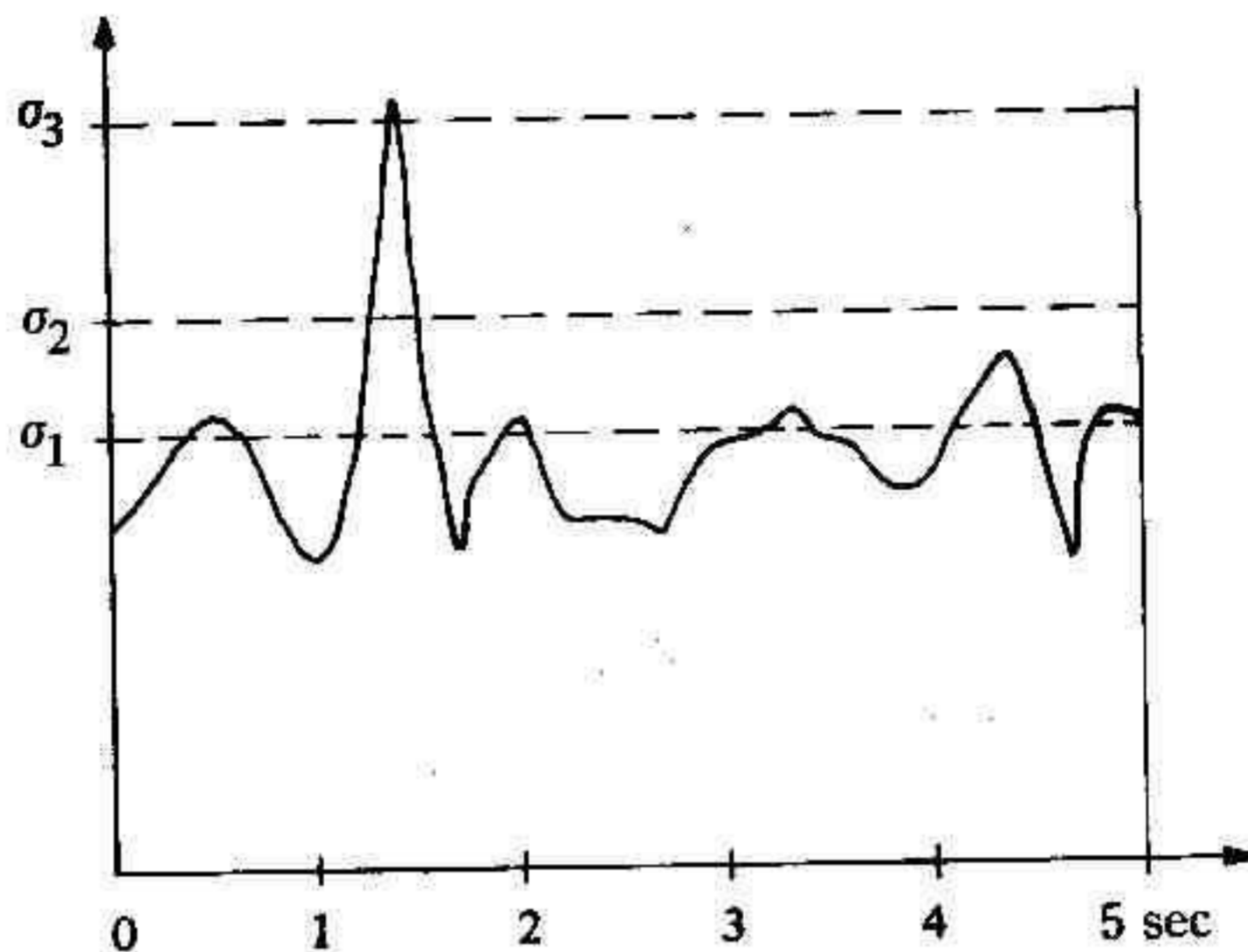


Fig. 5. Sigma meter circuit ( $\sigma$ )

The meter circuit selector (7) provides a choice of  $\sigma_1$  (32%),  $\sigma_2$  (4.5%) and  $\sigma_3$  (0.26%). To measure according to say  $\sigma_2$  (see Fig. 5), the following procedure is employed:

The meter circuit switch (7) is set to the  $\sigma_2$  position. The START pushbutton is operated. After approx. 5 sec. the FLUTTER meter (6) will deflect to a value that was exceeded for approx. 5% of the time of the measurement – that is, for approx. 0.25 sec. In other words: Random peaks occurring during less than 5% of the time of the measurement are not included in the result.

In practice, results of measurements when using the  $\sigma_2$  circuit are in fairly good agreement with results when using the DIN and DIN PEAK circuits.

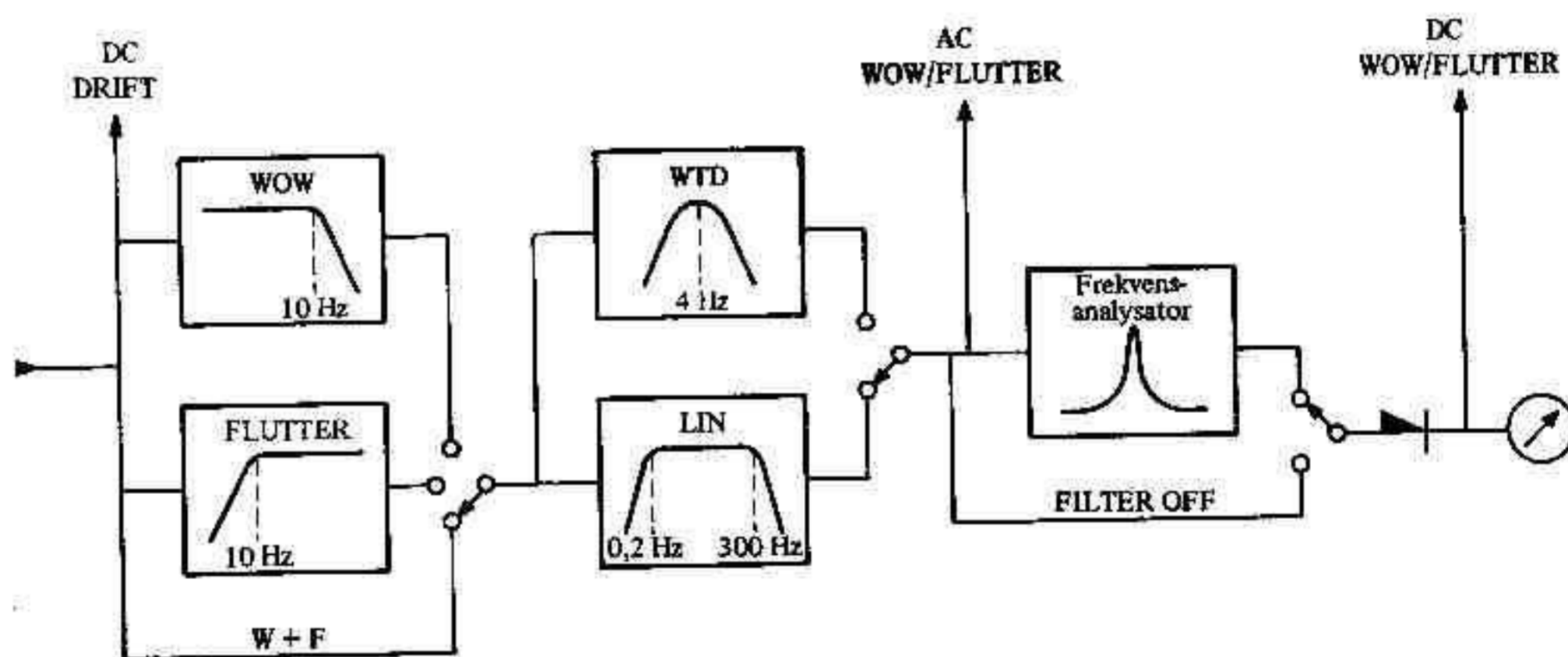


Fig. 6. Block diagram of the filter section of the WM1.

### Analysis of the Wow and Flutter Spectrum

In fault-finding work on record players and tape recorders in regard to wow and flutter, being able to make the right diagnosis is very important. This can be quite difficult if not impossible when using the



previously described measuring methods. To make such a diagnosis it is necessary to be able to measure the dominant frequencies selectively – that is, separately.

The WM1 incorporates a number of filters specially intended for such analysis of the wow and flutter spectrum (Fig. 6).

The frequency spectrum can be divided into wow and flutter depressing the WOW and FLUTTER buttons of the filter function switch (17). The crossover frequency is 10 Hz. Wow thus is defined as the frequencies below 10 Hz; and flutter is defined as the frequencies above 10 Hz (Fig. 7). The weighted filter is switched off by setting the filter function switch (17) to the LIN position, providing linear measurement of the frequency spectrum.

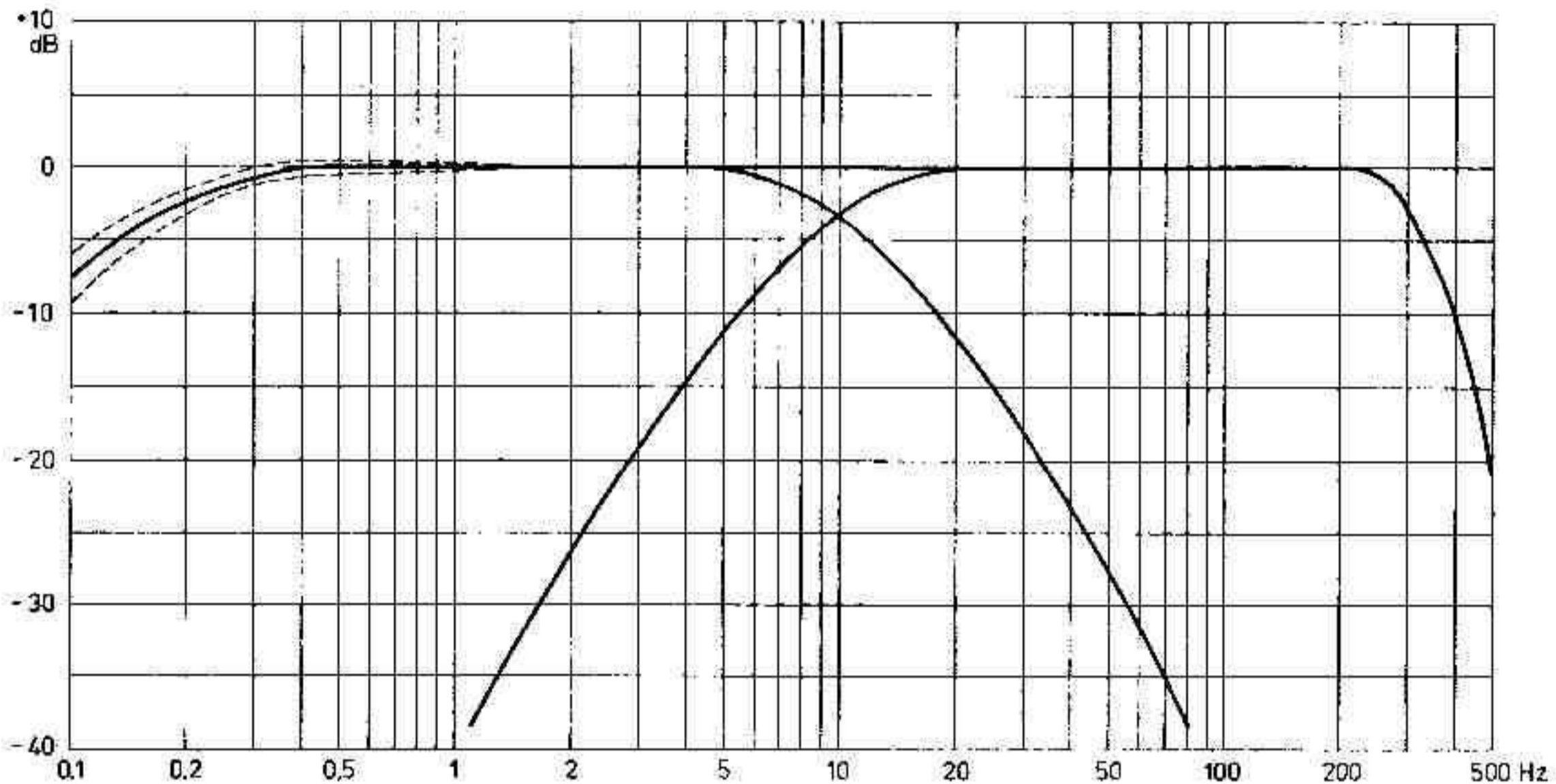


Fig. 7. Wow and flutter filter, linear (WOW, FLUTTER and W+F).

The wow and flutter spectrum is measured with the frequency analyser (9) and (10) which is a selective variable bandpass filter having a frequency range of 1 Hz ... 316 Hz. This filter makes it possible to determine which wow and flutter frequencies are dominant and to predict, on the basis of this knowledge, which rotating components – idlers, belt drive, motor, bearings etc. – should be repaired or replaced as the case may be. The manufacturer of the instrument in question is normally willing to supply information about the connection between the dominant frequencies and the rotating components. Note that the filter is relatively sluggish in the lowest ranges (1 ... 3.16 Hz and 3.16 ... 10 Hz), due to its high Q. Hence the filter should be varied slowly in these ranges so that it will have time to »swing« into place.

#### Monitor Outputs (Fig. 6)

On the back of the WM1 are three BNC outputs for oscilloscope, ink-recorder, analyser or some other form of monitor:

1. The DC DRIFT output voltage is analogous to the DRIFT meter (3) deflection and is equal to  $\pm 1$  V DC at full scale.
2. The AC WOW/FLUTTER output voltage is analogous to the FLUTTER meter (6) deflection and identical to the wow and flutter signal before the frequency analyser (see Fig. 6). The WOW, FLUTTER, WTD and LIN filters may thus be employed in conjunction with this output. For sine-wave modulated wow and flutter the output voltage is equal to 1 V AC at full scale.
3. The DC WOW/FLUTTER output voltage is analogous to the FLUTTER meter (6) deflection and identical to the rectified signal after the meter circuit (Fig. 7). The output voltage is equal to 1 V DC at full scale.

Pin No.	Designation	Function (see Figs. 2 and 3)	Remark
1			Not connected
2	DRIFT OFFSET	(4)	Control voltage: $\pm 1$ V/%
3	START	(8)	
4	0.03%	WOW/ FLUTTER range (16)	
5	0.1%		
6	0.3%		
7	1%		
8	3%		
9	0.3%	DRIFT range (1)	
10	1%		
11	3%		
12	10%		
13	DIN	Meter circuit(7)	
14	DIN PEAK		
15	$\sigma 1$		
16	$\sigma 2$		
17	$\sigma 3$		
18	WOW	Filter function (17)	
19	FLUTTER		
20		Chassis	
21	DRIFT DC	Analog output (18)	$\pm 1$ V DC at full scale
22	WOW/FLUTTER	Analog output (19)	1 V AC at full scale
23	WOW/FLUTTER	Analog output (20)	1 V DC at full scale
24		Analyser frequency (9)	Control voltage, $V_C = 0 \dots +10$ V $f_u = (1 + 0.216 V_C) f_n$ $f_l$ = lower filter frequency in range of interest
25	NO INPUT	Level indicator	High (on): + 15 V Low (off): - 15 V Load: max. 470 k $\Omega$
26			Not connected
27			Not connected
28			Not connected
29	FILTER OFF	(10)	
30	1 ... 3.16 Hz	Analyser frequency range (10)	
31	3.16 ... 10 Hz		
32	10 ... 31.6 Hz		
33	31.6 ... 100 Hz		
34	100 ... 316 Hz		
35	WTD	Filter function (17)	
36	LIN		
37	W + F		

## **Remote Control**

The WM1 is prepared for remote control of all functions and ranges. If this facility is desired, the instrument should be sent to the factory at Struer, Denmark, for installation of a number of control circuits and a 37-pole connector, REMOTE (21).

The meaning of the individual pins of the REMOTE connector (21) appears from the table. The functions and levels listed are activated at »high« level (3, 4 ... 15 V) and not activated at »low« level (0 ... 0.4) unless otherwise specified.

## **CIRCUIT ANALYSIS**

The Wow/Flutter WM1 consists broadly of the following sections:

- (1) Input stage (3.15 kHz)
- (2) Frequency detector (0.2 Hz ... 300 Hz)
- (3) Filters (wow, flutter and weighted)
- (4) Meter circuit according to DIN 45507, sigma circuit, and start-up automatic control circuit.
- (5) Frequency analyser (1 Hz ... 316 Hz)

**Input stage.** The input signal passes through the emitter follower TR1 and is thereafter stepped up by a factor of approx. 230 in the AC amplifier consisting of TR2, TR3 and TR4.

Then follow a 3rd-order highpass filter buffered by TR5 and a 3rd-order lowpass filter buffered by TR6. These filters constitute a 6th-order bandpass filter with 3150 Hz as centre frequency. Unwanted frequencies are thus prevented from reaching the detector circuit.

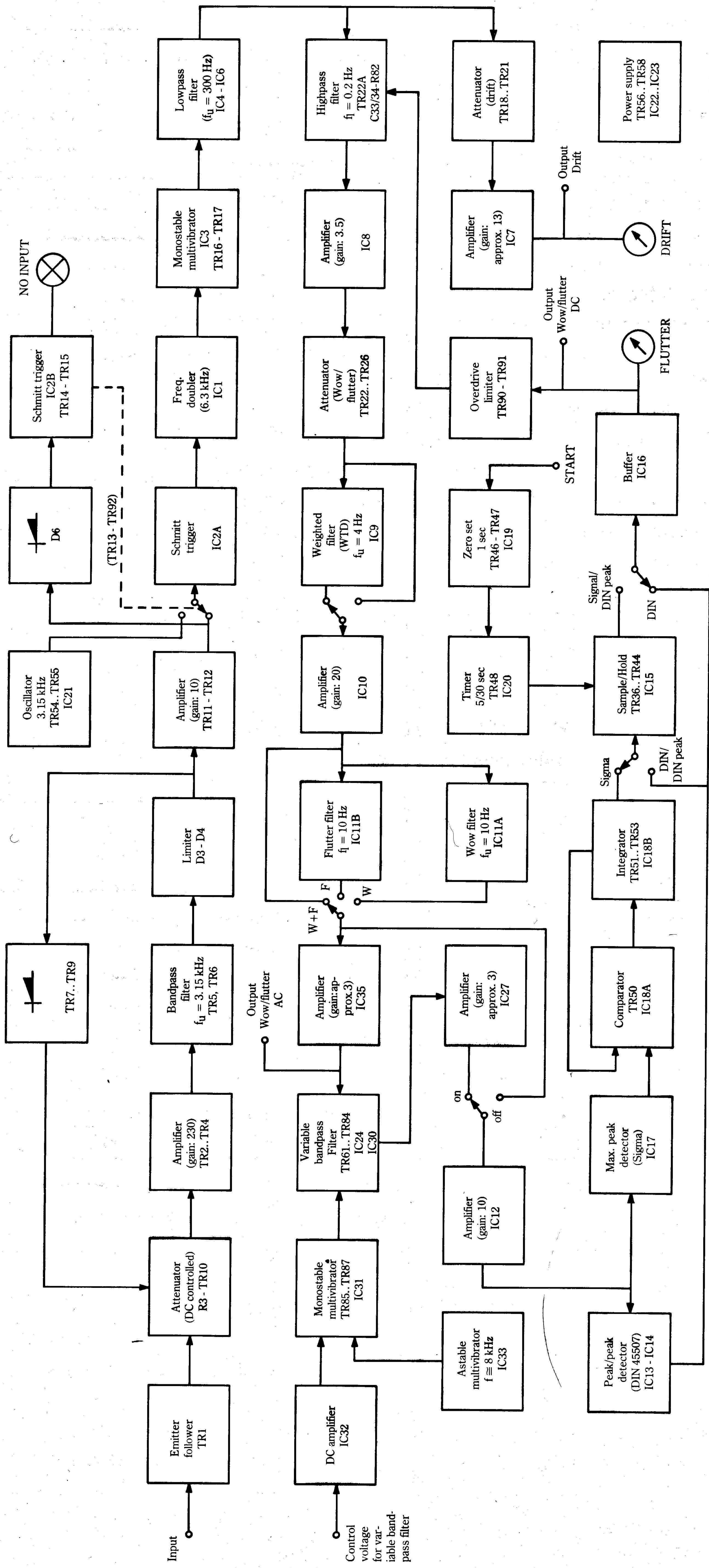


Fig. 8 Block diagram.

The signal is limited by D3 and D4, whereafter TR11 and TR12 match the level to the Schmitt trigger IC2A. The square-wave pulses at the output of IC2A are differentiated across capacitors C20 and C21. Furthermore, a doubling of frequency is obtained by means of the two NOR-gates IC1A and IC1B.

**Automatic cut-in of the internal oscillator.** When the input signal is too low, the internal oscillator switches on automatically. The Schmitt trigger IC2B senses on the peak-rectified input signal and controls TR15, which turns on the NO INPUT lamp on the front panel simultaneously with TR14 going on. TR14 in turn controls FET switches TR23 and TR92, which feed the external or the internal signal, respectively, to IC2A.

**AGC control.** Overdriving at powerful input levels is prevented by an AGC circuit comprising TR7 ... TR10 such that the signal is first rectified and smoothed by TR8, C17 and C18 whereafter it, via the buffer, controls TR10 which clamps the signal to chassis potential between C2 and C3.

**Frequency detector.** The frequency detector consists of a monostable multivibrator followed by a 5th-order Butterworth lowpass filter which attenuates the fundamental by approx. 120 dB (the fundamental after doubling is 6.3 kHz). The filter's 3 dB frequency is 300 Hz, and its output level will be proportional to the immediate number of input pulses arriving from the monostable multivibrator. At the filter output it will therefore be possible to register frequency variations having a bandwidth of 300 Hz. To ensure stable amplitude of the pulses from the monostable multivibrator the signal is shaped by TR17. The lowpass filter is composed of a 1st-order section (IC5) and two 2nd-order sections (IC6A and IC6B). Offset adjustment of drift is carried out via the inverting input of IC5.

**DC and AC attenuators.** From the output of the lowpass filter the signal is fed to the DC and AC attenuators, respectively, controlled by means of FET switches. IC7 is buffer and output amplifier for the DC signal. The output signal is  $\pm 1$  V, corresponding to full-scale deflection on the drift meter. Before the AC signal passes through the attenuator, its DC component is filtered off by C33 and C34 which combine with R82 to form a time constant that is sufficiently large to secure a total lower band limit of 0.2 Hz. IC8 buffers this RC network in addition to providing a gain of approx. 3.5.

**Weighted filter.** The weighted filter (WTD) is built up around IC9, and TR27 and TR28 provide a means of selecting between weighted and linear operation. IC10 operates as buffer for the FET switches and steps up the signal by a factor of 20. The level at the output is approx. 350 mV at full scale.

**Wow and flutter filter.** The wow filter (IC11A) and flutter filter (IC11B) is a 2nd-order Butterworth lowpass and highpass filter, respectively, with 10 Hz as 3 dB frequency. FET switches TR29, TR30 and TR31 cut in the W + F, WOW and FLUTTER filters, respectively. FET switches TR32 and TR33 provide a means of selecting whether you want to use the variable bandpass filter or not. IC12 buffers the FET switches and provides a gain of 10.

**Meter circuit (DIN 45507).** Rectification of the AC signal according to DIN 45507 occurs in IC13 and IC14 so that the positive peak value will lie across C45 and the negative one across C47. IC14A functions as summing amplifier; its output will be an expression of the peak-to-peak value of the AC signal seeing that the charging time constant is approx. 20 times lower than the discharge time constant.

**Meter circuit (sigma).** Before entering the sigma circuit, the signal is full-wave rectified in IC7A and IC17B. The actual rectification is done in IC17A whilst IC17B sums the positive and negative halfwaves. Both in this rectifier and in the one described above the negative feedback voltage is taken off after the diodes for which reason the diode voltage drop is reduced by approximately the open-loop gain of the operational amplifiers.

The sigma circuit consists of a comparator (IC18A) controlling an integrator (IC18B). Whether positive or negative integration is carried out depends on whether the output voltage across C48 is greater or smaller than the input voltage at the non-inverting input of IC18A. The integration rate depends on which resistor – R157 ( $\sigma$  1), R160 ( $\sigma$  2) or R161 ( $\sigma$  3) – has been cut in. TR35 and TR45 are used for zero-setting the circuit, C48 being discharged and the input of IC18A connected to chassis potential.

**Automatic Start-up control circuit.** Measurement involving use of the automatic start-up control circuit may be used with DIN measurements and is always used in sigma measurements.

The circuit consists of a timer (IC19 and IC20) controlling a peak-rectifying sample and held circuit (IC15). Rectification is performed via TR41A which operates as a diode having very low leakage current; this causes C50 to be charged up to the maximum voltage presents within a measuring period. TR43 and TR44 are inserted as buffers so as not to load C50.

Feedback voltage for IC15 is taken from the emitter of TR44 to eliminate the voltage drop across TR41A, TR43 and TR44. D34 prevents the output of IC15 from going into negative saturation and so turn TR41 on when not wanted. TR42A also functions as a diode.

A measuring operation may be divided into three periods:

- (1) Zero setting, approx. 1 sec.
- (2) Sampling, lasting 5 sec for sigma measurements and approx. 30 sec. for DIN PEAK measurements.
- (3) Retaining the result of the measurement until the next triggering.

When the START button is operated, the trigger signal enters R143 in the form of a positive voltage pulse which triggers the monostable multivibrator IC19. This delivers the zero set pulse of approx. 1 sec, during which period FET switches TR35, TR45, TR41, TR42 and TR38 go on, thereby zero-setting the circuits.

The negative flank of the first pulse triggers the next monostable multivibrator IC20, which delivers the sampling pulse. This results in the following changes from before: TR45, TR35 and TR41 go off, and the circuit is ready to measure the maximum voltage arriving from the sigma or DIN meter circuit.

On the negative flank of the sampling pulse the circuit goes into the »hold« state, causing TR42 and TR38 to go off. The charge on C50 can now no longer be changed, and the meter locking caused by TR38 ceases.

Changing the time constant from 5 sec to 30 sec is carried out by means of TR49, which is on only during sigma measurements. In DIN PEAK measurements, during which TR36 and TR39 are on, the meter time constant is simulated by the network composed of R125 and C49 which is necessary to preserve correct dynamic conditions.

**Frequency analyser.** The frequency analyser is composed of two 2nd-order bandpass filters of the state-variable type. Because these filters are identical except that their centre frequency is 7% off-tune, a description of the one section will suffice.

Range switching is carried out by means of FET switches TR62 ... TR66 and TR68 ... TR72 in such a manner that they are on pairwise. For example, in the range from 100 Hz to 316 Hz it is TR62 and TR68 which are on.

Continuous variation of the frequency will be possible by altering the values of all resistors in series with the FET switches which have been cut into the circuit. This introduces certain difficulties in practice for which reason a different solution was chosen.

The resistors instead of being varied are cut in and out at a frequency of approx. 8 kHz, and by varying the cut-in and cut-out times the same effect is obtained as would have resulted from altering the resistors, and the result is a change in frequency. Cut-in and cut-out are carried out by means of TR61 and TR67, controlled by TR87.

An astable multivibrator, IC33, generates the switch signal. It triggers a monostable multivibrator the pulse width of which is controllable by means of a DC voltage.

By charging C82 with a constant current a linear change of the mark-to-space ratio as a function of control voltage is obtained. P12 and P13 are used to adjust the voltage so that a change from 0 to 10 V at R239 produces a frequency change of 3.16 times (10 dB).

**Overdrive limiter.** Heavy overdriving causes the time constant generated by C33, C34 and R82 to keep the meter in saturation for a relatively long time. This is remedied by a circuit (TR90 and TR91) which senses on the meter output. At a level corresponding to 1.5 times at full scale, TR22A is switched on, causing the time constant to be reduced by a factor of approx. 500.

**3.15 kHz oscillator.** The oscillator employs IC21 as amplifying device and is of the Wien bridge type. TR54 peak-rectifies the output signal, and the smoothed voltage across C62 controls the gate of TR55 which serves as a variable resistor. The gain will adjust itself so that the amplitude of the output voltage becomes equal to the sum of the voltage drop across D53 plus the base-emitter voltage across TR54.

**Power supply.** The plus supply uses an integrated regulator, IC22, with a built-in reference voltage and current limiter.

The output voltage from the series transistor TR56 is inverted in IC23 and furnishes, at the output of series transistor TR57, the negative supply. The current limiter for the latter is TR58, which removes control voltage from TR57 when the voltage drop across R181 is approx. 0.6 V.

## ADJUSTMENTS

The Wow/Flutter Meter WM1 is designed for operation for long periods of time without readjustments and maintenance. Only in the case of component faults it will normally be necessary to check and adjust the instrument. In that case the following procedure should be observed.

Only those adjustments are described which can be carried out with normally available instruments. The remaining adjustments require special test equipment for which reason the instrument should be sent to the factory if such adjustments are necessary.

The adjustments described require the following instruments:

1. Digital voltmeter, AC/DC, accuracy better than 0.1%.
2. Audio generator, 1 kHz ... 10 kHz.
3. Frequency counter, 1 kHz ... 10 kHz, accuracy better than  $5 \times 10^{-6}$ .

### Adjustment of the Internal Oscillator and the Drift Meter Circuit

1. Check the mechanical zero ( $\approx 0$ ) on the drift meter (3).
- 2.

Operate the following pushbuttons:

Drift range (1):	0.3%
Meter circuit (7):	DIN
Filter characteristic (17):	W+F and LIN
Wow/flutter range (16):	1%
Frequency analyser (10):	OFF

3. Allow the instrument to warm up for not less than half an hour with its cabinet closed.
4. Remove the top cover.
5. Check the +17 V potential in the power supply and if necessary adjust with potentiometer P10 on circuit board A (see Fig. 9). Check  $\pm 17$  V potential.
6. Connect a frequency counter to the 3.15 kHz output (11), and with potentiometer P9 on circuit board A adjust the oscillator frequency to exact value of 3.15 kHz.
7. Short-circuit the centre pin of the drift potentiometer (4) to chassis potential and adjust the deflection of the drift meter (3) to 0 with potentiometer P1 on circuit board B.

8. Remove short-circuit. Set drift potentiometer (4) to 0. When switching between the 0.3% and 10% ranges (1) the drift meter (3) should show a constant reading of 0. This reading is adjusted in the 0.3% range with the FINE potentiometer (2) and in the 10% range with potentiometer P2 on circuit board B.
9. Set the drift range switch (1) to 0.3% position. Adjust drift meter (3) reading to 0 using drift potentiometer (4) and, if necessary, FINE potentiometer (2). Thereafter set the range switch (1) to 10% position.
10. Connect an audio generator to one of the inputs, say (12), and adjust frequency to exactly 3.465 (3.15 kHz + 10%), checking with a frequency counter.

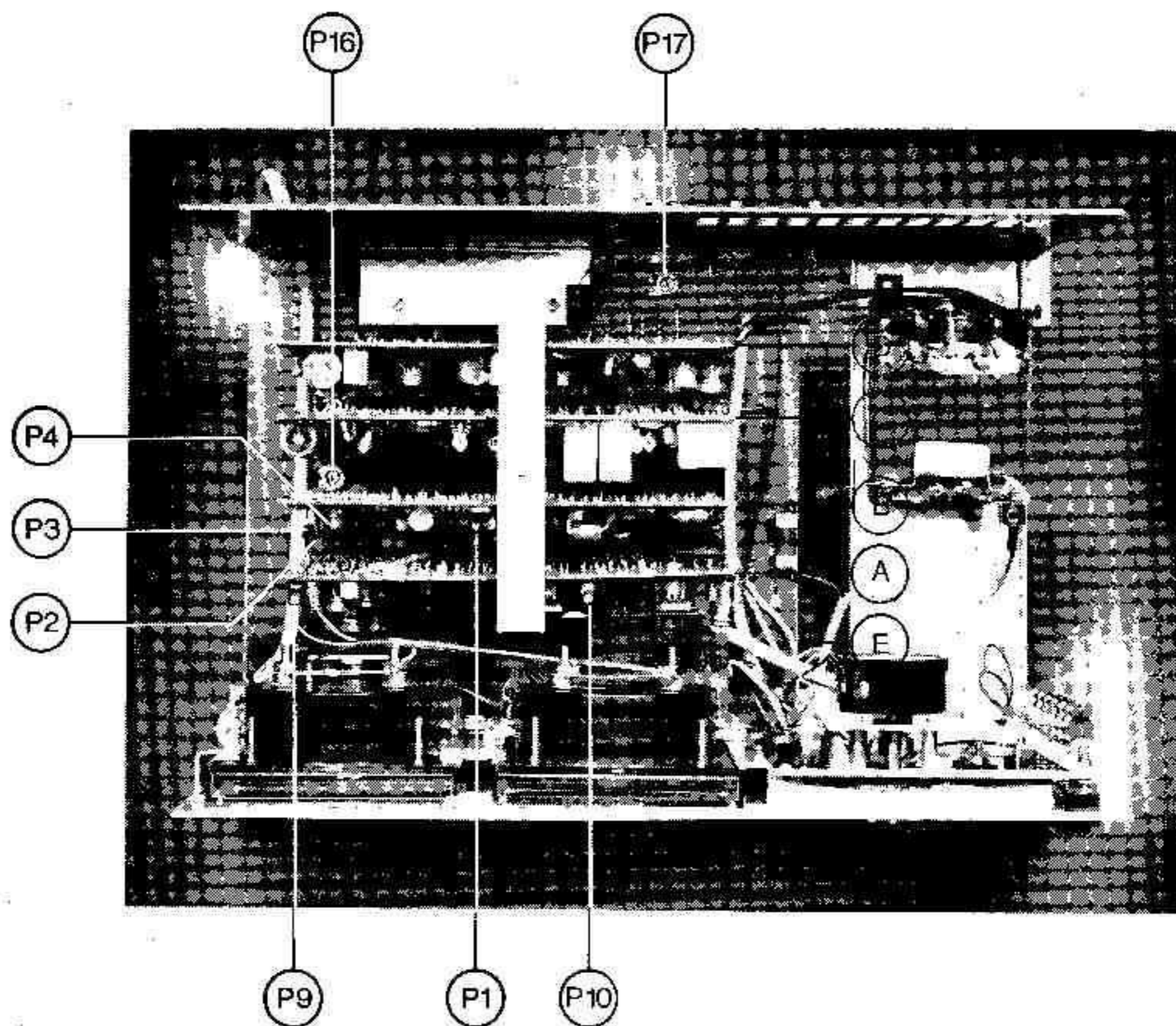


Fig. 9. Adjustment.

11. Connect a digital voltmeter to the drift analog output (18) and adjust the output voltage to 1 V DC with potentiometer P3 on circuit board B.
12. With potentiometer P16 on circuit board E (bottom board) adjust drift meter (3) to read +10%.

#### **Adjustment of Frequency Analyser (9)**

1. Connect a digital voltmeter to the centre pin of filter potentiometer (9). Voltage at this point should be capable of being varied from 0 to +10 V by turning the dial from 1 to 3.16.
2. Turn the dial against the left end stop. Then turn the dial slowly clockwise, checking if the voltage at the potentiometer centre pin only just begins to rise smoothly (from 0 V) at 1 on the dial scale. If it does not, adjust the knob with respect to the shaft.
3. Thereafter turn the dial clockwise to 3.16 on the outer scale. Voltage at the potentiometer centre pin should then be +10 V; correction, if necessary, may be made with the potentiometer P17 on the bottom board.



**PARTS LIST**

R1	5010045	Resistor	47 K $\Omega$	5%	0.125 W
R2	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R3	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R4	5010144	Resistor	680 $\Omega$	5%	0.125 W
R5	5010063	Resistor	150 K $\Omega$	5%	0.125 W
R6	5010064	Resistor	2.2 K $\Omega$	5%	0.125 W
R7	5010083	Resistor	270 K $\Omega$	5%	0.125 W
R8	5010064	Resistor	2.2 K $\Omega$	5%	0.125 W
R9	5010144	Resistor	680 $\Omega$	5%	0.125 W
R10	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R11	5010045	Resistor	47 K $\Omega$	5%	0.125 W
R12	5010069	Resistor	3.9 K $\Omega$	5%	0.125 W
R13	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R14	5010083	Resistor	270 K $\Omega$	5%	0.125 W
R15	5010075	Resistor	33 K $\Omega$	5%	0.125 W
R16	5010141	Resistor	27 K $\Omega$	5%	0.125 W
R17	5010141	Resistor	27 K $\Omega$	5%	0.125 W
R18	5010062	Resistor	68 K $\Omega$	5%	0.125 W
R19	5010075	Resistor	33 K $\Omega$	5%	0.125 W
R20	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R21	5010075	Resistor	33 K $\Omega$	5%	0.125 W
R22		Resistor	24.9 K $\Omega$	1%	0.125 W
R23	5010141	Resistor	27 K $\Omega$	5%	0.125 W
R24	5010141	Resistor	27 K $\Omega$	5%	0.125 W
R25	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R26	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R27	5010091	Resistor	82 K $\Omega$	5%	0.125 W
R28	5010066	Resistor	1.8 K $\Omega$	5%	0.125 W
R29	5010075	Resistor	33 K $\Omega$	5%	0.125 W
R30	5010045	Resistor	47 K $\Omega$	5%	0.125 W
R31	5010064	Resistor	2.2 K $\Omega$	5%	0.125 W
R32	5010064	Resistor	2.2 K $\Omega$	5%	0.125 W
R33	5010091	Resistor	82 K $\Omega$	5%	0.125 W
R34	5010076	Resistor	3.3 K $\Omega$	5%	0.125 W
R35	5010411	Resistor	47 $\Omega$	5%	0.125 W
R36		Resistor	1.2 M $\Omega$	5%	0.125 W
R37		Resistor	562 K $\Omega$	1%	0.125 W
R38		Resistor	100 K $\Omega$	1%	0.125 W
R39		Resistor	10 K $\Omega$	1%	0.125 W
R40		Resistor	1 K $\Omega$	1%	0.125 W
R41	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R42	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R44	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R45	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R45A	5010045	Resistor	47 K $\Omega$	5%	0.125 W
R46	5010065	Resistor	100 $\Omega$	5%	0.125 W
R47	5010141	Resistor	27 K $\Omega$	5%	0.125 W
R48	5010068	Resistor	820 $\Omega$	5%	0.125 W
R49	5010048	Resistor	4.7 K $\Omega$	5%	0.125 W
R50	5010058	Resistor	470 $\Omega$	5%	0.125 W
R51	5010058	Resistor	470 $\Omega$	5%	0.125 W
R52	5010064	Resistor	2.2 K $\Omega$	5%	0.125 W
R53	5010067	Resistor	560 K $\Omega$	5%	0.125 W
R53A	5010067	Resistor	3.3 K $\Omega$	5%	0.125 W
R54	5010064	Resistor	2.2 K $\Omega$	5%	0.125 W
R55	5010048	Resistor	4.7 K $\Omega$	5%	0.125 W
R56		Resistor	13.7 K $\Omega$	1%	0.125 W
R57		Resistor	402 K $\Omega$	1%	0.125 W
R58		Resistor	124 K $\Omega$	1%	0.125 W
R59	5010059	Resistor	10 K $\Omega$	5%	0.125 W

R60	5010048	Resistor	4.7 K $\Omega$	5%	0.125 W
R61		Resistor	2.87 K $\Omega$	1%	0.125 W
R62		Resistor	18.7 K $\Omega$	1%	0.125 W
R63		Resistor	280 K $\Omega$	1%	0.125 W
R64	5010054	Resistor	1 M $\Omega$	5%	0.125 W
R65		Resistor	18.7 K $\Omega$	1%	0.125 W
R66	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R67		Resistor	18.7 K $\Omega$	1%	0.125 W
R68		Resistor	18.7 K $\Omega$	1%	0.125 W
R69		Resistor	7.15 K $\Omega$	1%	0.125 W
R70		Resistor	9.76 K $\Omega$	1%	0.125 W
R71		Resistor	18.7 K $\Omega$	1%	0.125 W
R72		Resistor	18.7 K $\Omega$	1%	0.125 W
R73		Resistor	10 K $\Omega$	1%	0.125 W
R74		Resistor	3.83 K $\Omega$	1%	0.125 W
R75		Resistor	3.16 K $\Omega$	1%	0.125 W
R76		Resistor	1 K $\Omega$	1%	0.125 W
R77		Resistor	316 $\Omega$	1%	0.125 W
R78		Resistor	147 $\Omega$	1%	0.125 W
R79	5010045	Resistor	47 K $\Omega$	5%	0.125 W
R80		Resistor	4.99 K $\Omega$	1%	0.125 W
R81		Resistor	60.4 K $\Omega$	1%	0.125 W
R82	5010047	Resistor	120 K $\Omega$	5%	0.125 W
R82A	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R83		Resistor	110 K $\Omega$	1%	0.125 W
R84		Resistor	225 K $\Omega$	1%	0.125 W
R85		Resistor	3.16 K $\Omega$	1%	0.125 W
R86		Resistor	1 K $\Omega$	1%	0.125 W
R87		Resistor	316 $\Omega$	1%	0.125 W
R88		Resistor	100 $\Omega$	1%	0.125 W
R89		Resistor	46.4 $\Omega$	1%	0.125 W
R90		Resistor	402 K $\Omega$	1%	0.125 W
R91		Resistor	402 K $\Omega$	1%	0.125 W
R92		Resistor	130 K $\Omega$	1%	0.125 W
R93		Resistor	267 K $\Omega$	1%	0.125 W
R94		Resistor	294 K $\Omega$	1%	0.125 W
R95		Resistor	5.23 K $\Omega$	1%	0.125 W
R96		Resistor	100 K $\Omega$	1%	0.125 W
R97		Resistor	158 K $\Omega$	1%	0.125 W
R98		Resistor	158 K $\Omega$	1%	0.125 W
R99		Resistor	6.19 K $\Omega$	1%	0.125 W
R100		Resistor	3.65 K $\Omega$	1%	0.125 W
R101		Resistor	3.65 K $\Omega$	1%	0.125 W
R102		Resistor	6.98 K $\Omega$	1%	0.125 W
R103		Resistor	158 K $\Omega$	1%	0.125 W
R104		Resistor	158 K $\Omega$	1%	0.125 W
R105		Resistor	6.19 K $\Omega$	1%	0.125 W
R106		Resistor	3.65 K $\Omega$	1%	0.125 W
R107		Resistor	3.65 K $\Omega$	1%	0.125 W
R108		Resistor	6.98 K $\Omega$	1%	0.125 W
R109	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R109A	5010054	Resistor	1 M $\Omega$	5%	0.125 W
R110		Resistor	54.9 K $\Omega$	1%	0.125 W
R111		Resistor	20 K $\Omega$	1%	0.125 W
R112		Resistor	182 K $\Omega$	1%	0.125 W
R113		Resistor	29.4 K $\Omega$	1%	0.125 W
R114		Resistor	8.87 K $\Omega$	1%	0.125 W
R115		Resistor	14.7 K $\Omega$	1%	0.125 W
R116		Resistor	54.9 K $\Omega$	1%	0.125 W
R117		Resistor	100 K $\Omega$	1%	0.125 W
R118		Resistor	100 K $\Omega$	1%	0.125 W
R119		Resistor	4.87 K $\Omega$	1%	0.125 W

R120		Resistor	4.87 K $\Omega$	1%	0.125 W
R121		Resistor	10 K $\Omega$	1%	0.125 W
R122		Resistor	10 K $\Omega$	1%	0.125 W
R123		Resistor	10 K $\Omega$	1%	0.125 W
R124		Resistor	10 K $\Omega$	1%	0.125 W
R125		Resistor	4.99 K $\Omega$	1%	0.125 W
R126		Resistor	2.67 K $\Omega$	1%	0.125 W
R126A		Resistor	20 K $\Omega$	1%	0.125 W
R127	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R128	5010053	Resistor	15 K $\Omega$	5%	0.125 W
R129	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R130	5010298	Resistor	2.7 K $\Omega$	5%	0.125 W
R131	5010053	Resistor	15 K $\Omega$	5%	0.125 W
R131A	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R132	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R133		Resistor	54.9 K $\Omega$	1%	0.125 W
R134		Resistor	10 K $\Omega$	1%	0.125 W
R135		Resistor	10 K $\Omega$	1%	0.125 W
R136		Resistor	100 K $\Omega$	1%	0.125 W
R137		Resistor	100 K $\Omega$	1%	0.125 W
R138		Resistor	100 K $\Omega$	1%	0.125 W
R139		Resistor	100 K $\Omega$	1%	0.125 W
R140		Resistor	100 K $\Omega$	1%	0.125 W
R141		Resistor	88.7 K $\Omega$	1%	0.125 W
R142	5010059	Resistor	10 K $\Omega$	1%	0.125 W
R142A	5010040	Resistor	1 K $\Omega$	1%	0.125 W
R143	5010059	Resistor	10 K $\Omega$	1%	0.125 W
R144	5010045	Resistor	47 K $\Omega$	1%	0.125 W
R145	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R145A	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R146	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R147	5010075	Resistor	33 K $\Omega$	5%	0.125 W
R148	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R149	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R150	5010053	Resistor	15 K $\Omega$	5%	0.125 W
R151	5010073	Resistor	390 K $\Omega$	5%	0.125 W
R152		Resistor	1.5 M $\Omega$	5%	0.125 W
R153	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R154	5010053	Resistor	15 K $\Omega$	5%	0.125 W
R155	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R156	5010047	Resistor	120 K $\Omega$	5%	0.125 W
R157		Resistor	6.19 K $\Omega$	1%	0.125 W
R158		Resistor	2 K $\Omega$	1%	0.125 W
R159	5010052	Resistor	6.8 K $\Omega$	5%	0.125 W
R160		Resistor	39.2 K $\Omega$	1%	0.125 W
R161		Resistor	649 K $\Omega$	1%	0.125 W
R162		Resistor	243 K $\Omega$	0,25%	0.125 W
R163	5010068	Resistor	820 K $\Omega$	5%	0.125 W
R164	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R165		Resistor	249 K $\Omega$	0.25%	0.125 W
R166	5010247	Resistor	1.5 K $\Omega$	5%	0.125 W
R168		Resistor	2 K $\Omega$	1%	0.125 W
R169	5010411	Resistor	47 $\Omega$	5%	0.125 W
R170	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R171	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R172	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R173	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R174		Resistor	5.62 K $\Omega$	1%	0.125 W
R175		Resistor	1.2 K $\Omega$	10%	1 W
R176		Resistor	6.04 K $\Omega$	1%	0.125 W
R177		Resistor	6.04 K $\Omega$	1%	0.125 W

R178	5010069	Resistor	3.9 K $\Omega$	5%	0.125 W
R179		Resistor	10 K $\Omega$	1%	0.125 W
R180		Resistor	6.04 K $\Omega$	1%	0.125 W
R181		Resistor	2.2 $\Omega$	10%	1 W
R182	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R183	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R184	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R185	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R186	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R187		Resistor	4.99 K $\Omega$	1%	0.125 W
R188		Resistor	20 K $\Omega$	1%	0.125 W
R189	5010041	Resistor	5.6 K $\Omega$	5%	0.125 W
R190		Resistor	20 K $\Omega$	1%	0.125 W
R191		Resistor	4.99 K $\Omega$	0.25%	0.125 W
R192		Resistor	15.8 K $\Omega$	0.25%	0.125 W
R193		Resistor	49.9 K $\Omega$	0.25%	0.125 W
R194		Resistor	158 K $\Omega$	0.25%	0.125 W
R195		Resistor	499 K $\Omega$	0.25%	0.125 W
R196	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R197	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R198	5010041	Resistor	5.6 K $\Omega$	5%	0.125 W
R200	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R201		Resistor	4.64 K $\Omega$	0.25%	0.125 W
R202		Resistor	14.7 K $\Omega$	0.25%	0.125 W
R203		Resistor	46.4 K $\Omega$	0.25%	0.125 W
R204		Resistor	147 K $\Omega$	0.25%	0.125 W
R205		Resistor	464 K $\Omega$	0.25%	0.125 W
R206	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R207		Resistor	137 K $\Omega$	1%	0.125 W
R208		Resistor	100 K $\Omega$	1%	0.125 W
R209		Resistor	37.4 K $\Omega$	1%	0.125 W
R210		Resistor	20 K $\Omega$	1%	0.125 W
R211		Resistor	20 K $\Omega$	1%	0.125 W
R212		Resistor	1.62 K $\Omega$	1%	0.125 W
R213	5010041	Resistor	5.6 K $\Omega$	5%	0.125 W
R214		Resistor	4.99 K $\Omega$	1%	0.125 W
R215	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R216		Resistor	4.64 K $\Omega$	0.25%	0.125 W
R217		Resistor	14.7 K $\Omega$	0.25%	0.125 W
R218		Resistor	46.4 K $\Omega$	0.25%	0.125 W
R219		Resistor	147 K $\Omega$	0.25%	0.125 W
R220		Resistor	20 K $\Omega$	1%	0.125 W
R221		Resistor	20 K $\Omega$	1%	0.125 W
R222	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R223	5010041	Resistor	5.6 K $\Omega$	5%	0.125 W
R225	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R226	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R227		Resistor	4.32 K $\Omega$	0.25%	0.125 W
R228		Resistor	13.7 K $\Omega$	0.25%	0.125 W
R229		Resistor	43.2 K $\Omega$	0.25%	0.125 W
R230		Resistor	137 K $\Omega$	0.25%	0.125 W
R231		Resistor	432 K $\Omega$	5%	0.125 W
R232		Resistor	8.45 K $\Omega$	1%	0.125 W
R233		Resistor	5.49 K $\Omega$	1%	0.125 W
R234	5010048	Resistor	4.7 K $\Omega$	5%	0.125 W
R235	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R236	5010040	Resistor	1 K $\Omega$	5%	0.125 W
R237		Resistor	14 K $\Omega$	1%	0.125 W
R238		Resistor	2 K $\Omega$	2%	0.125 W
R239	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R240		Resistor	4.99 K $\Omega$	1%	0.125 W

R241		Resistor	2.1 K $\Omega$	1%	0.125 W
R242		Resistor	3.09 K $\Omega$	1%	0.125 W
R243		Resistor	27 K $\Omega$	1%	0.125 W
R250		Resistor	1.62 K $\Omega$	1%	0.125 W
R251	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R252	5010045	Resistor	47 K $\Omega$	5%	0.125 W
R253	5010059	Resistor	10 K $\Omega$	5%	0.125 W
R254	5010153	Resistor	1.2 K $\Omega$	5%	0.125 W
R256		Resistor	10 K $\Omega$	1%	0.125 W
R257		Resistor	1.78 K $\Omega$	1%	0.125 W
R258		Resistor	37.4 K $\Omega$	1%	0.125 W
R259	5010065	Resistor	100 $\Omega$	5%	0.125 W
R260		Resistor	13.3 K $\Omega$	1%	0.125 W
R261		Resistor	93.1 K $\Omega$	1%	0.125 W
R262		Resistor	25.5 K $\Omega$	1%	0.125 W
R263		Resistor	10 K $\Omega$	1%	0.125 W
R264		Resistor	18.2 K $\Omega$	1%	0.125 W
R265		Resistor	10 K $\Omega$	1%	0.125 W
R266	5010053	Resistor	15 K $\Omega$	5%	0.125 W
R267	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R268	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R269	5010117	Resistor	330 K $\Omega$	5%	0.125 W
R270		Resistor	8.45 K $\Omega$	1%	0.125 W
R271		Resistor	8.66 K $\Omega$	1%	0.125 W
R272	5001022	Resistor	390 $\Omega$	5%	0.5 W
R273	5010049	Resistor	-100 K $\Omega$	5%	0.125 W
R274	5001007	Resistor	39 $\Omega$	10%	0.5 W
R275	5001007	Resistor	39 $\Omega$	10%	0.5 W
R276		Resistor	13,3 K $\Omega$	1%	0.125 W
R277	5010049	Resistor	100 K $\Omega$	5%	0.125 W
R278		Resistor	422 K $\Omega$	1%	0.125 W

P1		Potentiometer, TR	10 K $\Omega$ -lin		0,5W
P2		Potentiometer, TR	10 K $\Omega$ -lin		0,5 W
P3		Potentiometer, TR	10 K $\Omega$ -lin		0,5 W
P4		Potentiometer, TR	50 K $\Omega$ -lin		0,5 W
P5		Potentiometer, TR	1 K $\Omega$ -lin		0,1 W
P6		Potentiometer, TR	1 K $\Omega$ -lin		0,1 W
P7		Potentiometer, TR	1 K $\Omega$ -lin		0,1 W
P8		Potentiometer, TR	50 K $\Omega$ -lin		0,1 W
P9		Potentiometer, TR	20 K $\Omega$ -lin		0,5 W
P10		Potentiometer, TR	10 K $\Omega$ -lin		0,5 W
P11		Potentiometer, TR	50 K $\Omega$ -lin		0,5 W
P12		Potentiometer, TR	2 K $\Omega$ -lin		0,5 W
P13		Potentiometer, TR	1 K $\Omega$ -lin		0,5 W
P15	5370000	Potentiometer, TR	250 $\Omega$ -lin		0,1 W
P16	5370000	Potentiometer, TR	250 $\Omega$ -lin		0,1 W
P17	5370168	Potentiometer, TR	5 K $\Omega$ -lin		0.1 W
P18		Potentiometer, TR	25 K $\Omega$ -lin		3 W
P19		Potentiometer, TR	25 K $\Omega$ -lin		3 W
P20		Potentiometer, TR	470 $\Omega$ -lin		0.25 W

C1	4133011	Capacitor, MK	10 nF	10%	250 V
C2	4100029	Capacitor, PS	2.2 nF	5%	63 V
C3	4133012	Capacitor, MK	150 nF	20%	250 V
C4	4101007	Capacitor, PS	220 pF	5%	63 V
C5	4200108	Capacitor, Elko Tant	4.7 $\mu$ F		25 V
C6	4200101	Capacitor, Elko Tant	10 $\mu$ F		16 V
C6A	4201041	Capacitor, Elko Tant	6.8 $\mu$ F		40 V
C7	4101007	Capacitor, PS	220 pF	5%	63 V

C8	4133012	Capacitor, MK	150 nF	20%	250 V
C9	4000077	Capacitor, K. Pla	47 pF	2%	63 V
C10	4100058	Capacitor, PS	3.3 nF	2.5%	63 V
C11	4100058	Capacitor, PS	3.3 nF	2.5%	63 V
C12	4100058	Capacitor, PS	3.3 nF	2.5%	63 V
C13	4100029	Capacitor, PS	2.2 nF	5%	63 V
C14	4100029	Capacitor, PS	2.2 nF	5%	63 V
C15	4101018	Capacitor, PS	470 pF	5%	63 V
C16	4133004	Capacitor, MK	22 nF	20%	250 V
C17	4200108	Capacitor, Elko Tant	4.7 $\mu$ F		25 V
C18	4130100	Capacitor, MK	68 nF	10%	250 V
C18A	4130132	Capacitor, MK	100 nF	10%	250 V
C19	4201057	Capacitor, Elko Tant	1 $\mu$ F		35 V
C20	4010003	Capacitor, K. HK.	220 pF	20%	400 V
C21	4010003	Capacitor, K. HK.	220 pF	20%	400 V
C22	4100031	Capacitor, PS	4.7 nF	1%	63 V
C23	4010060	Capacitor, K. HK.	22 nF		40 V
C24	4010067	Capacitor, K. Pla	1.5 nF	10%	63 V
C25	4201058	Capacitor, Elko Tant	0.47 $\mu$ F		35 V
C26	4100048	Capacitor, PS	27 nF	1%	63 V
C27	4100048	Capacitor, PS	27 nF	1%	63 V
C28	4100048	Capacitor, PS	27 nF	1%	63 V
C29	4100048	Capacitor, PS	27 nF	1%	63 V
C30	4100048	Capacitor, PS	27 nF	1%	63 V
C31	4130136	Capacitor, MK	1 $\mu$ F	20%	100 V
C32	4200108	Capacitor, Elko Tant	4.7 $\mu$ F		25 V
C32A	4201041	Capacitor, Elko	6.8 $\mu$ F		40 V
C32B	4200100	Capacitor, Elko	22 $\mu$ F		40 V
C33	4200230	Capacitor, Elko Tant	15 $\mu$ F		16 V
C34	4200230	Capacitor, Elko Tant	15 $\mu$ F		16 V
C35	4230132	Capacitor, MK	100 nF	10%	250 V
C36	4130132	Capacitor, MK	100 nF	10%	250 V
C37		Capacitor, MK	1 $\mu$ F	5%	100 V
C38	4230132	Capacitor, MK	100 nF	10%	250 V
C38A	4130132	Capacitor, MK	100 nF	10%	250 V
C39	4130132	Capacitor, MK	100 nF	10%	250 V
C40	4130132	Capacitor, MK	100 nF	10%	250 V
C41	4200133	Capacitor, Elko	100 $\mu$ F		10 V
C42	4200098	Capacitor, Elko	100 $\mu$ F		6 V
C43		Capacitor, Elko	47 $\mu$ F		16 V
C44		Capacitor, Elko	47 $\mu$ F		16 V
C45		Capacitor, MK	4.7 $\mu$ F	5%	100 V
C46	4201058	Capacitor, Elko Tant	0.47 $\mu$ F		35 V
C47		Capacitor, MK	4.7 $\mu$ F	5%	100 V
C48	4200111	Capacitor, Elko	1000 $\mu$ F		10 V
C48A	4200230	Capacitor, Elko Tant	15 $\mu$ F		16 V
C49		Capacitor, Elko Tant	22 $\mu$ F		16 V
C49A	4011022	Capacitor, K. Pla	4.7 nF		40 V
C50	4134010	Capacitor, MK	470 nF	10%	400 v
C51	4133011	Capacitor, MK	10 nF	10%	250 V
C52	4200230	Capacitor, Elko Tant	15 $\mu$ F		16 V
C52A	4201041	Capacitor, Elko	6.8 $\mu$ F		40 V
C53	4133011	Capacitor, MK	10 nF	10%	250 V
C54	4200230	Capacitor, Elko Tant	15 $\mu$ F		16 V
C54A	4201041	Capacitor, Elko	6.8 $\mu$ F		40 V
C55	4000085	Capacitor, K. Pla	100 pF	2%	63 V
C56	4000085	Capacitor, K. Pla	100 pF	2%	63 V
C57	4000085	Capacitor, K. Pla	100 pF	2%	63 V
C58	4000085	Capacitor, K. Pla	100 pF	2%	63 V
C59	4000078	Capacitor, K. Pla	68 pF	2%	63 V
C60	4000078	Capacitor, K. Pla	68 pF	2%	63 V

C61	4200101	Capacitor, Elko Tant	10 $\mu$ F		16 V
C62	4201058	Capacitor, Elko Tant	0.47 $\mu$ F		35 V
C62A	4200016	Capacitor, Elko	22 $\mu$ F		25 V
C62B	4201041	Capacitor, Elko	6.8 $\mu$ F		40 V
C63	4200101	Capacitor, Elko Tant	10 $\mu$ F		16 V
C64	4201074	Capacitor, Elko	47 $\mu$ F		40 V
C65	4010041	Capacitor, K. Plaq	10 nF		40 V
C66	4200108	Capacitor, Elko Tant	4.7 $\mu$ F		25 V
C67	4200174	Capacitor, Elko	470 $\mu$ F		25 V
C68	4200332	Capacitor, Elko	2200 $\mu$ F		25 V
C69	4201074	Capacitor, Elko	47 $\mu$ F		40 V
C70		Capacitor, PS	320 nF	1%	63 V
C73		Capacitor, PS	2.2 nF	1%	63 V
C74	4200101	Capacitor, Elko Tant	10 $\mu$ F		16 V
C75	4200101	Capacitor, Elko Tant	10 $\mu$ F		16 V
C76	4130132	Capacitor, MK	100 nF	10%	250 V
C77		Capacitor, PS	320 nF	1%	63 V
C78		Capacitor, PS	2.2 nF	1%	63 V
C81	4010067	Capacitor, K. Plaq	1.5 nF	10%	63 V
C82	4100031	Capacitor, PS	4.7 nF	1%	63 V
C83	4100031	Capacitor, PS	4.7 nF	1%	63 V
C84	4200099	Capacitor, Elko	100 $\mu$ F		16 V
C85	4200099	Capacitor, Elko	100 $\mu$ F		16 V
C86	4200100	Capacitor, Elko	22 $\mu$ F		40 V
C87	4200100	Capacitor, Elko	22 $\mu$ F		40 V
C88	4200100	Capacitor, Elko	22 $\mu$ F		40 V
C89	4010060	Capacitor, K. HK.	22 nF		40 V
C90	4134010	Capacitor, MK	470 nF	10%	400 V
C91	4011025	Capacitor, K. Plaq	3.3 nF	10%	100 V
C92	4011025	Capacitor, K. Plaq	3.3 nF	10%	100 V
C95		Capacitor, Elko	100 $\mu$ F		16 V

D1...					
D6	8300058	Diode, Si		1N4148	
D6A	8300128	Diode, Zener		ZPD 5.6	
D7...					
D28	8300058	Diode, Si		1N4148	
D29	8300028	Diode, Zener		ZPD 9.1	
D30...					
D33	8300058	Diode, Si		1N4148	
D34	8300028	Diode, Zener		ZPD 9.1	
D35...					
D39	8300058	Diode, Si		1N4148	
D40	8300209	Diode, Ge		AA144	
D41	8300209	Diode, Ge		AA144	
D42	8300058	Diode, Si		1N4148	
D43	8300058	Diode, Si		1N4148	
D43A	8300058	Diode, Si		1N4148	
D44...					
D46	8300058	Diode, Si		1N4148	
D48	8300058	Diode, Si		1N4148	
D49...					
D51	8300128	Diode, Zener		ZPD 5.6	
D52	8300058	Diode, Si		1N4148	
D53	8300222	Diode, Zener		ZPD 2.7	
D54	8300023	Diode, Si		1N4002	
D55	8300028	Diode, Zener		ZPD 9.1	
D56	8300023	Diode, Si		1N4002	
	8300155	Rectifier, Si		B40C800	
D57...					
D80	8300058	Diode, Si		1N4148	

D81	8300169	Diode, Zener	ZPD 5.1
D82	8300058	Diode, Si	1N4148
D90...			
D98	8300058	Diode, Si	1N4148
D99	8300128	Diode, Zener	ZPD 5.6
D100	8300058	Diode, Si	1N4148
D101	8300058	Diode, Si	1N4148
D102	8300058	Diode, Si	1N4148
D103	8300058	Diode, Si	1N4148
D104	8300195	Diode, LED	TIL209
TR...			
TR12	8320377	Transistor, NPN	BC547C
TR13		Transistor, FET	2N5462
TR14	8320076	Transistor, PNP	MPS6517
TR15	8320377	Transistor, NPN	BC547C
TR15A	8320295	Transistor, NPN	BC337
TR16	8320075	Transistor, NPN	MPS6515
TR17	8320075	Transistor, NPN	MPS6515
TR18...			
TR22	8320119	Transistor, FET	TIS88A
TR22A	8320119	Transistor, FET	TIS88A
TR23...			
TR33	8320119	Transistor, FET	TIS88A
TR34	8340025	Transistor, PNP	SPS5431
TR35...			
TR38		Transistor, FET	TIS74
TR39...			
TR40	8320119	Transistor, FET	TIS88A
TR41	8320119	Transistor, FET	TIS88A
TR41A	8320119	Transistor, FET	TIS88A
TR42	8320119	Transistor, FET	TIS88A
TR42A	8320119	Transistor, FET	TIS88A
TR43	8320119	Transistor, FET	TIS88A
TR44	8320137	Transistor, NPN	BC182A
TR45	8320119	Transistor, FET	TIS88A
TR46	8320075	Transistor, NPN	MPS6515
TR47	8320076	Transistor, PNP	MPS6517
TR48	8320076	Transistor, PNP	MPS6517
TR49	8320119	Transistor, FET	TIS88A
TR50	8320137	Transistor, NPN	BC182B
TR51...			
TR53		Transistor, FET	TIS74
TR54	8340025	Transistor, PNP	SPS5431
TR55		Transistor, FET	BF244C
TR56	8320258	Transistor, NPN	TIP31
TR57	8320257	Transistor, PNP	TIP32
TR58	8320076	Transistor, PNP	MPS6517
TR61	8320413	Transistor, FET	U1897E
TR62	8320413	Transistor, FET	U1897E
TR63...			
TR66	8320412	Transistor, FET	U1899E
TR67	8320413	Transistor, FET	U1897E
TR68	8320413	Transistor, FET	U1897E
TR69...			
TR72	8320412	Transistor, FET	U1899E
TR73	8320413	Transistor, FET	U1897E
TR74	8320413	Transistor, FET	U1897E
TR75...			
TR78	8320412	Transistor, FET	U1899E

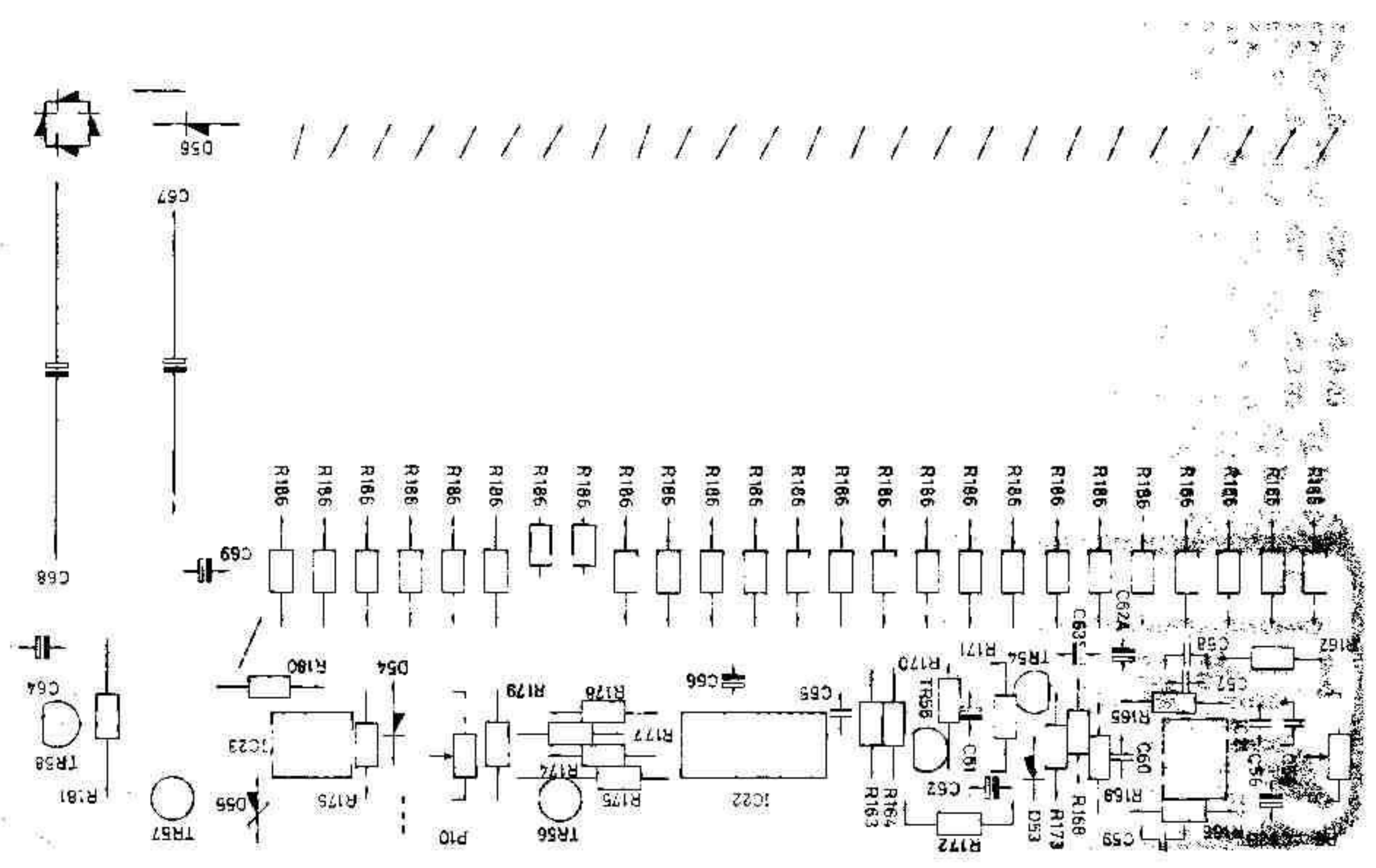


TR79	8320413	Transistor, FET	U1897E
TR80	8320413	Transistor, FET	U1897E
TR81...			
TR84	8320412	Transistor, FET	U1899E
TR85	8320076	Transistor, PNP	MPS6517
TR86	8320076	Transistor, PNP	MPS6517
TR87	8320323	Transistor, PNP	MPSA05
TR90	8320076	Transistor, PNP	MPS6517
TR91	8320075	Transistor, NPN	MPS6515
TR92	8320119	Transistor, FET	TIS88A

IC1		Quad 2 Input Nor Gate	SN 74LS02
IC2		Dual 4 Input Nand Schmitt Trigger	SN 74LS13
IC3	8340144	Timer	LM 555
IC4	8340039	Operational Amplifier	LM307
IC5	8340039	Operational Amplifier	LM 307
IC6	8340142	Dual Operational Amplifier	LM 1458
IC7	8340141	Operational Amplifier	LM 741
IC8	8340039	Operational Amplifier	LM 307
IC9	8340039	Operational Amplifier	LM 307
IC10	8340039	Operational Amplifier	LM 307
IC11	8340142	Dual Operational Amplifier	LM 1458
IC12	8340039	Operational Amplifier	LM 307
IC13	8340142	Dual Operational Amplifier	LM 1458
IC14	8340142	Dual Operational Amplifier	LM 1458
IC15	8340039	Operational Amplifier	LM 307
IC16	8340039	Operational Amplifier	LM 307
IC17	8340142	Dual Operational Amplifier	LM 1458
IC18	8340142	Dual Operational Amplifier	LM 1458
IC19	8340067	Timer	LM 555
IC20	8340067	Timer	LM 555
IC21	8340143	Operational Amplifier	LM 709
IC22	8340145	Voltage Regulator	LM 723
IC23	8340039	Operational Amplifier, FET	LM 307
IC24		Operational Amplifier, FET	CA 3140
IC25		Operational Amplifier, FET	CA 3140
IC26		Operational Amplifier, FET	CA 3140
IC27	8340039	Operational Amplifier, FET	LM 307
IC28		Operational Amplifier, FET	CA 3140
IC29		Operational Amplifier, FET	CA 3140
IC30		Operational Amplifier, FET	CA 3140
IC31	8340067	Timer	LM 555
IC32	8340048	Dual Operational Amplifier	LM 1458
IC33	8340067	Timer	LM 555
IC35	8340039	Operational Amplifier	LM 307

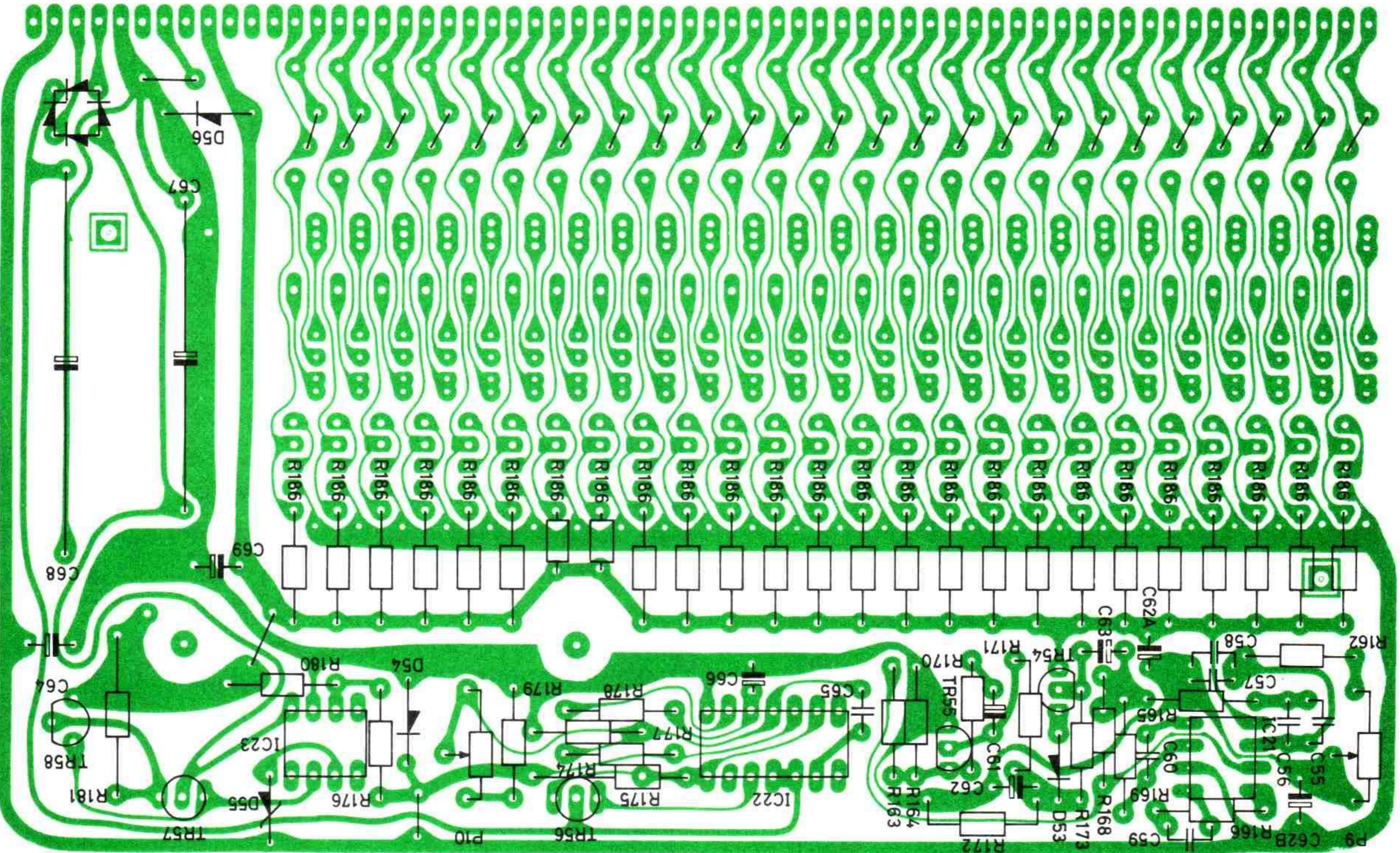
	Moving-coil meter, DRIFT	± 0.5 mA
	Moving-coil meter, FLUTTER	1 mA
8013178	Power transformer	2 × 19 V/0.3 A
6271086	Power cable	3 × 0.75 mm <sup>2</sup>
7400149	Switch filters	
7400150	Switch Meter circuit	
7400150	Switch Wow range	
7400151	Switch Drift range	
7400153	Switch Frequency analyser	
7200039	Fuseholder	
6600031	Fuse	80 mA slow
7210182	Terminal screw, red	3026003
7210181	Terminal screw, black	3026003
7210184	BNC socket	50 Ω
7212007	DIN socket, 5 pole	

Parts layout for circuit board A.  
Power supply, oscillator etc. (TR54 ...  
TR60, IC21 ... IC23).

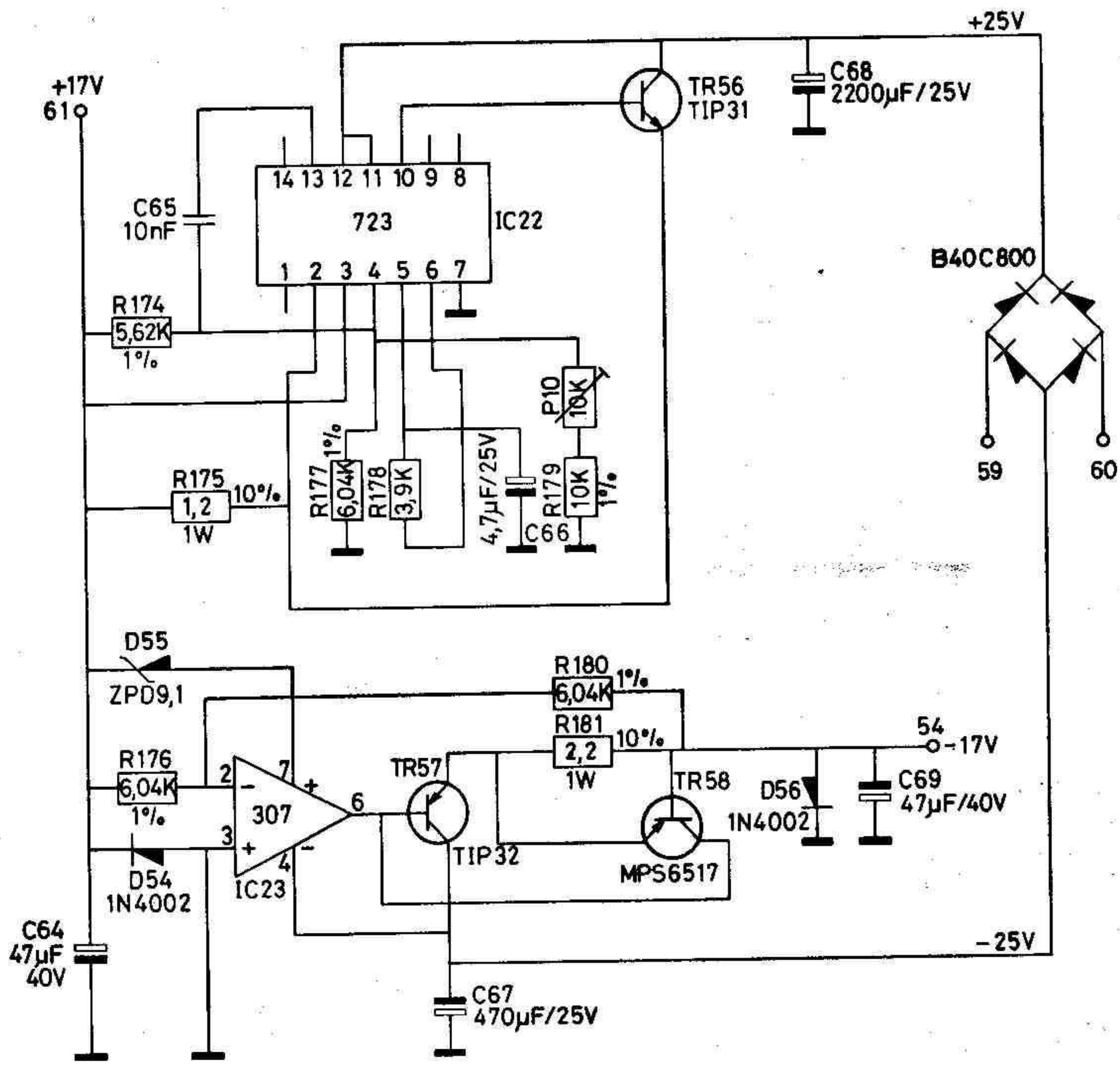


Knob FINE  
Knob Drift-Offset  
Knob Frekv. analyzator  
Rubber foot  
Manual  
0585027

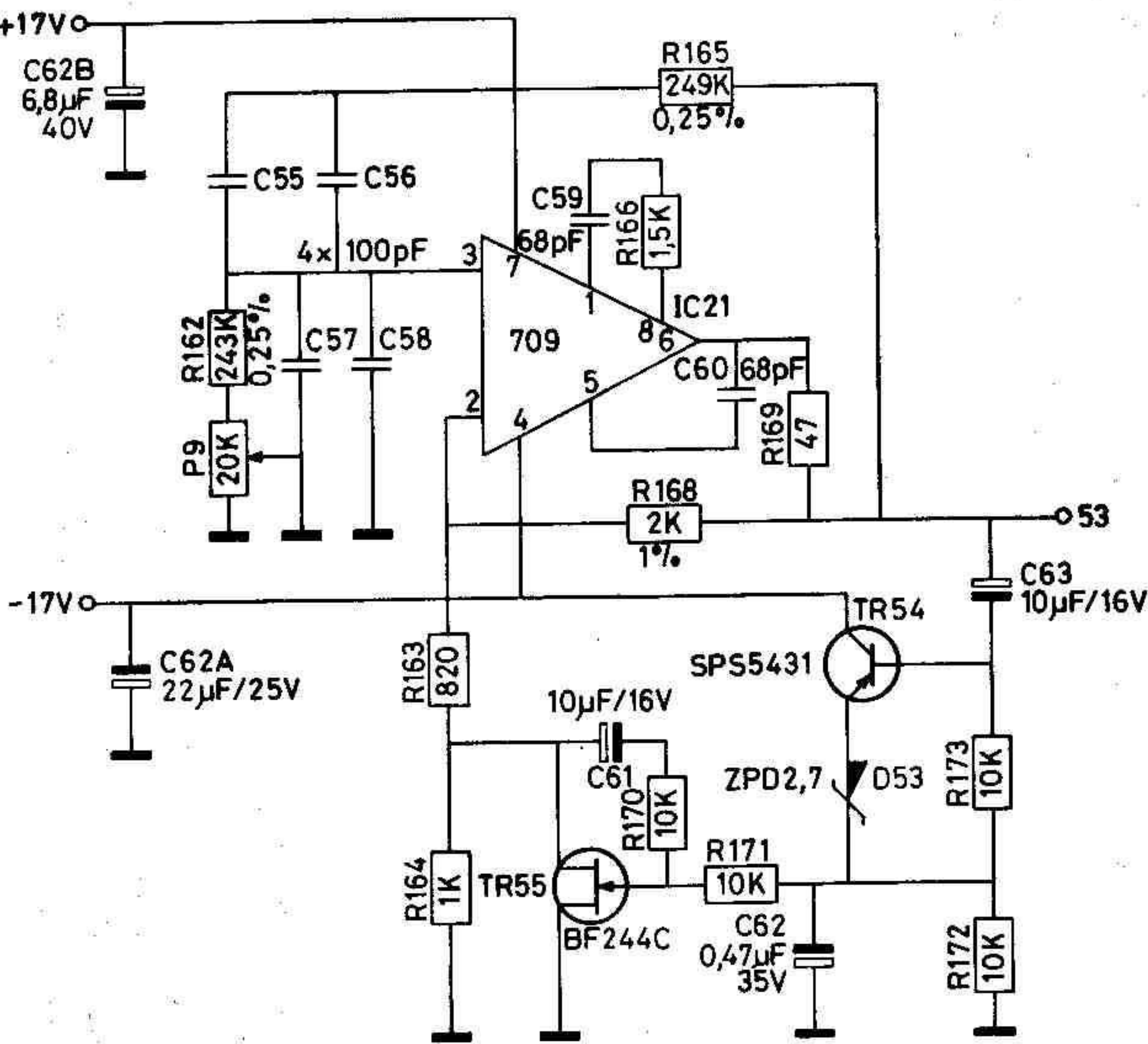
020-2320/040-1020  
020-4420/040-4020/042-4400  
020-6420/040-6020  
WMI



Power Supply



3,15KHz Oscillator



25 x FET-Switch Driver.

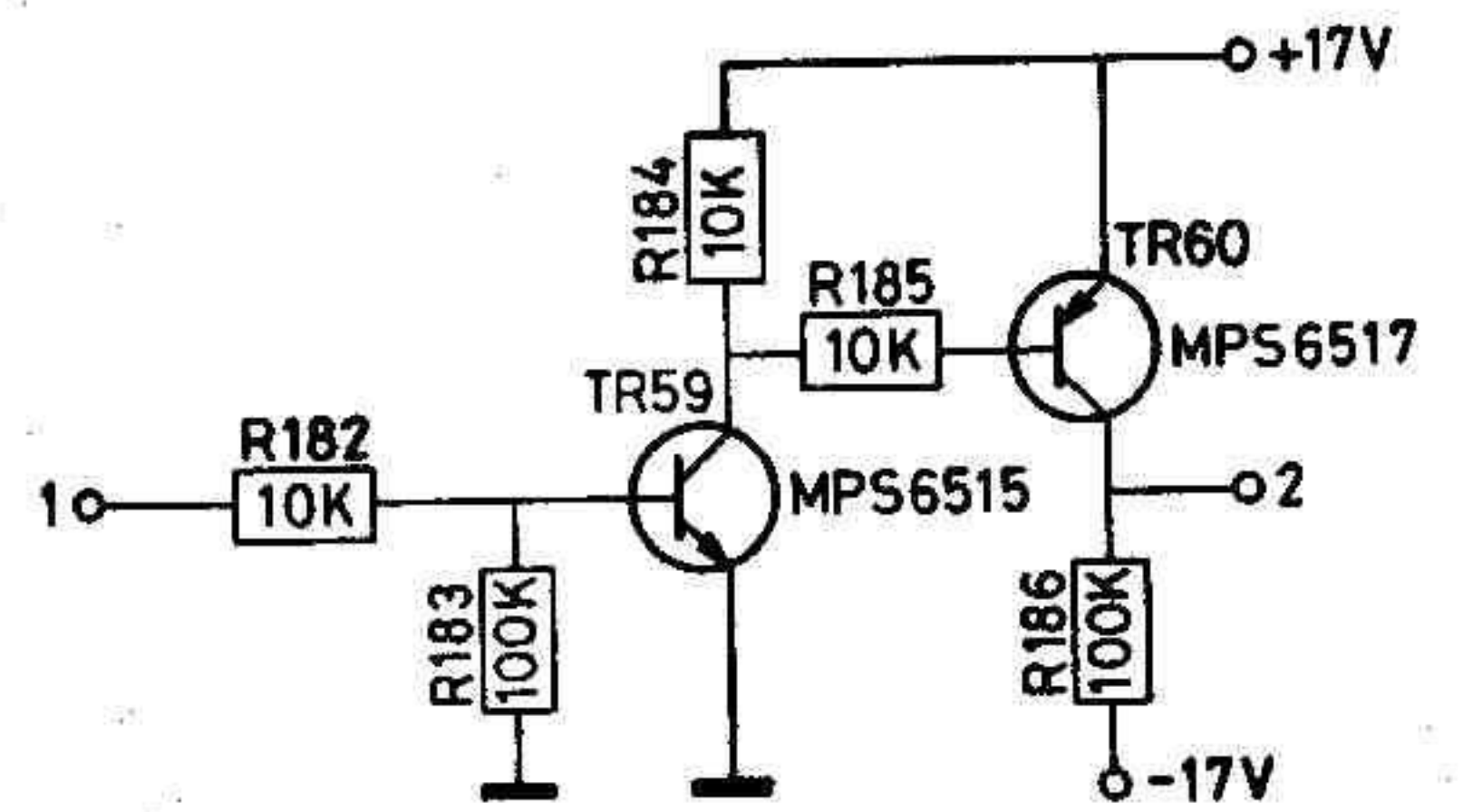
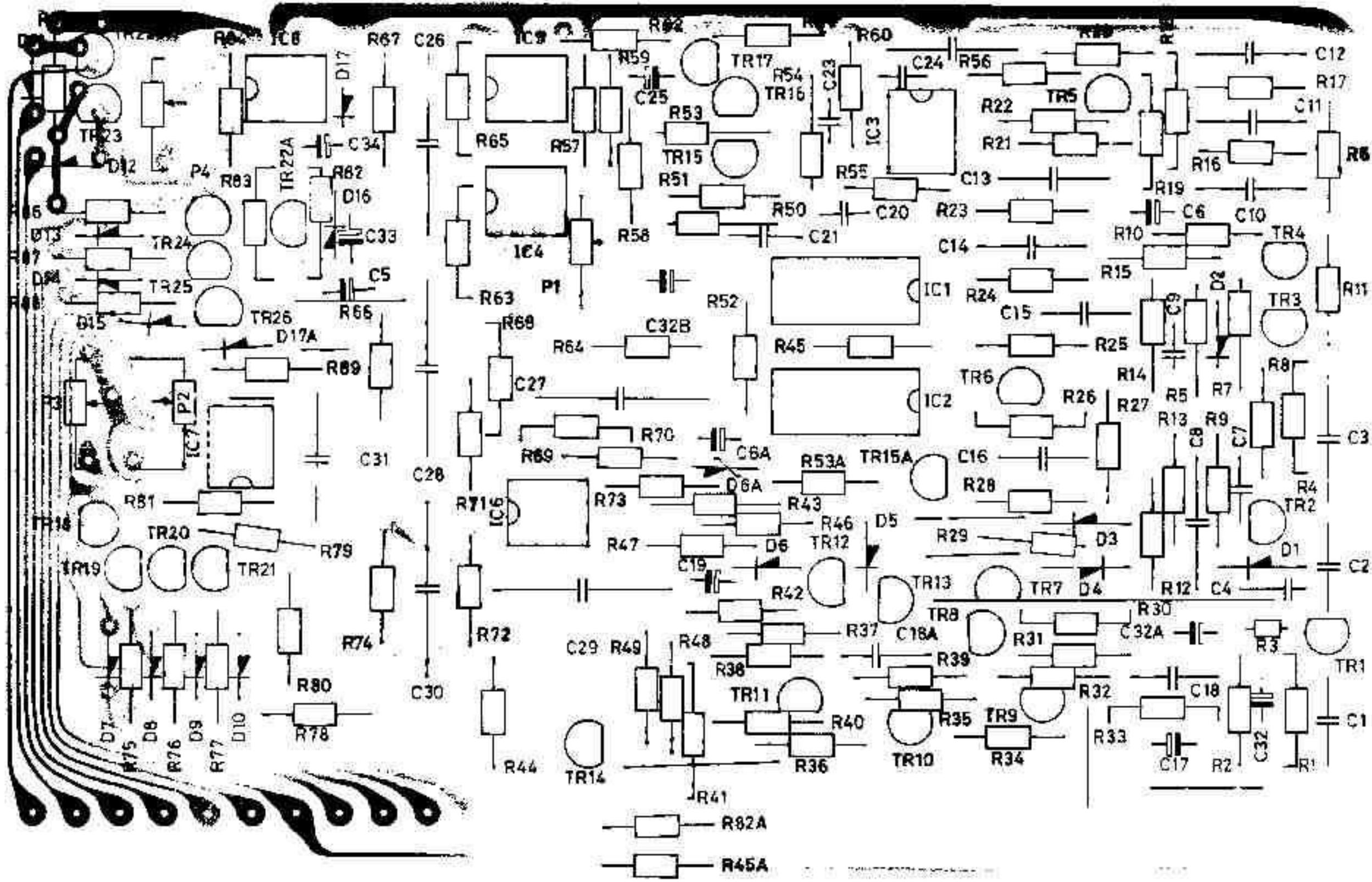
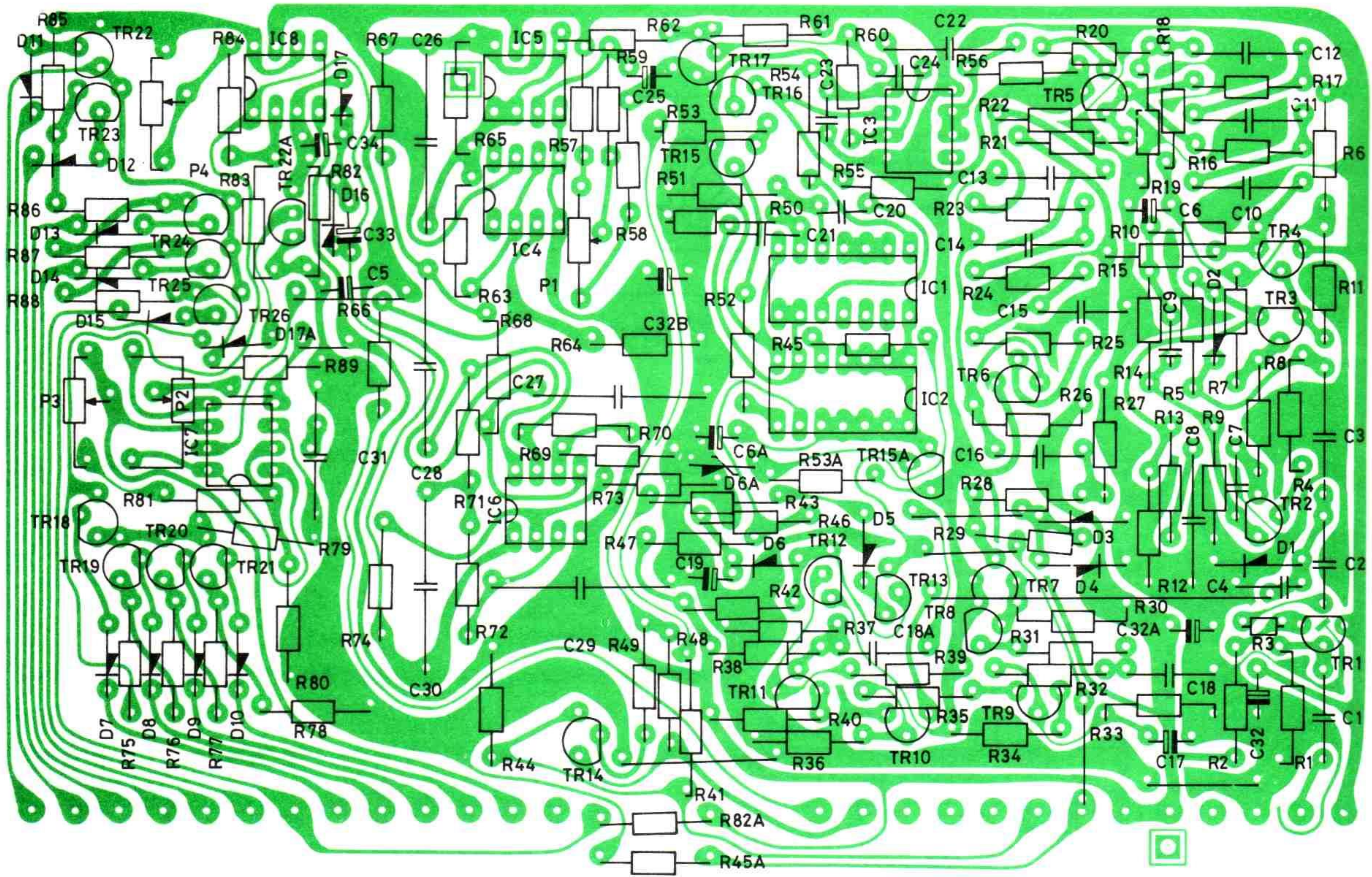


Diagram for circuit board A.  
Power supply, oscillator etc. (TR54...TR60,  
IC21...IC23).



**Parts layout for circuit board B.**  
 Input stage, detector, attenuator etc.  
 (TR1...TR26, IC1...IC8).



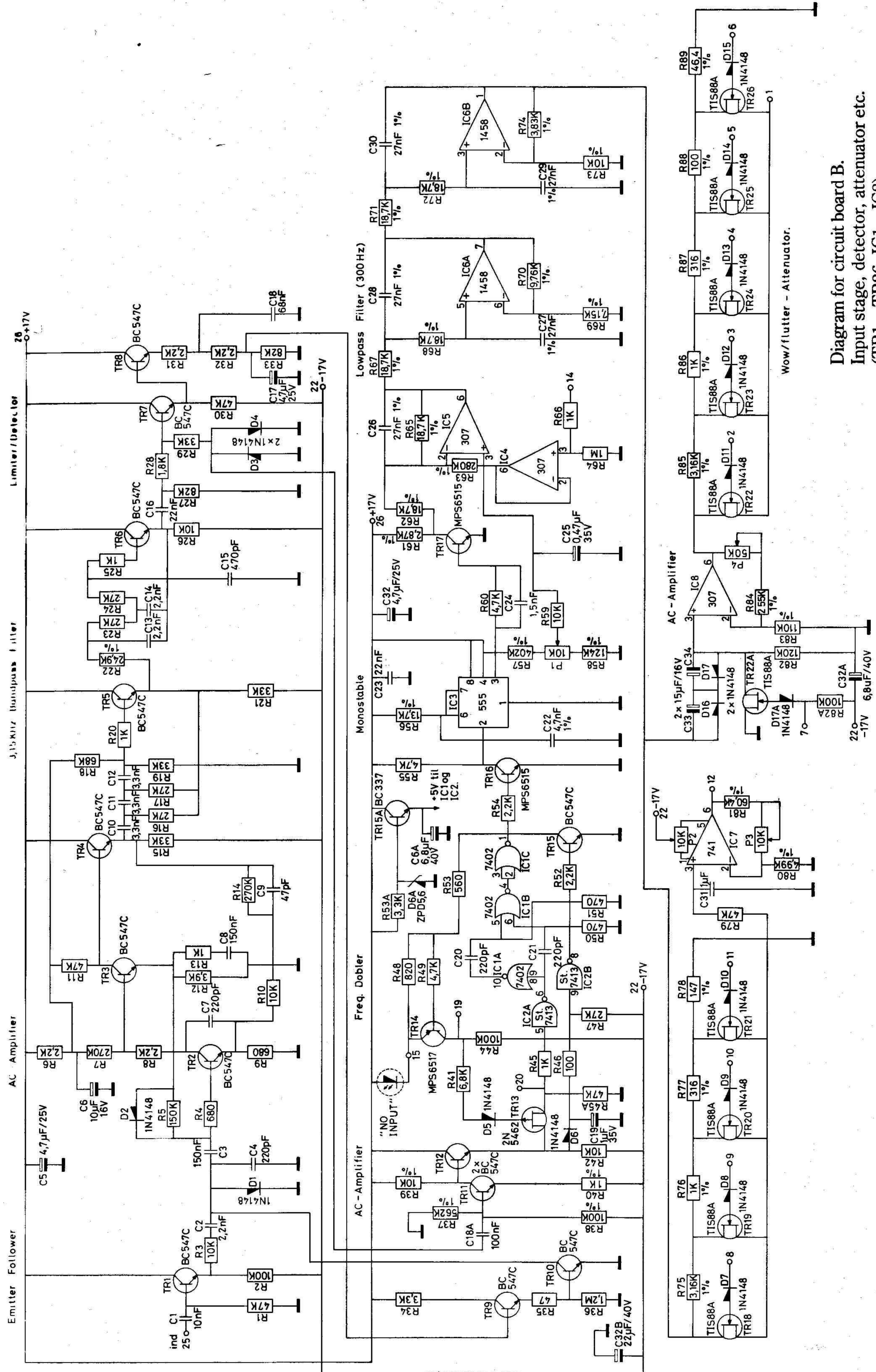
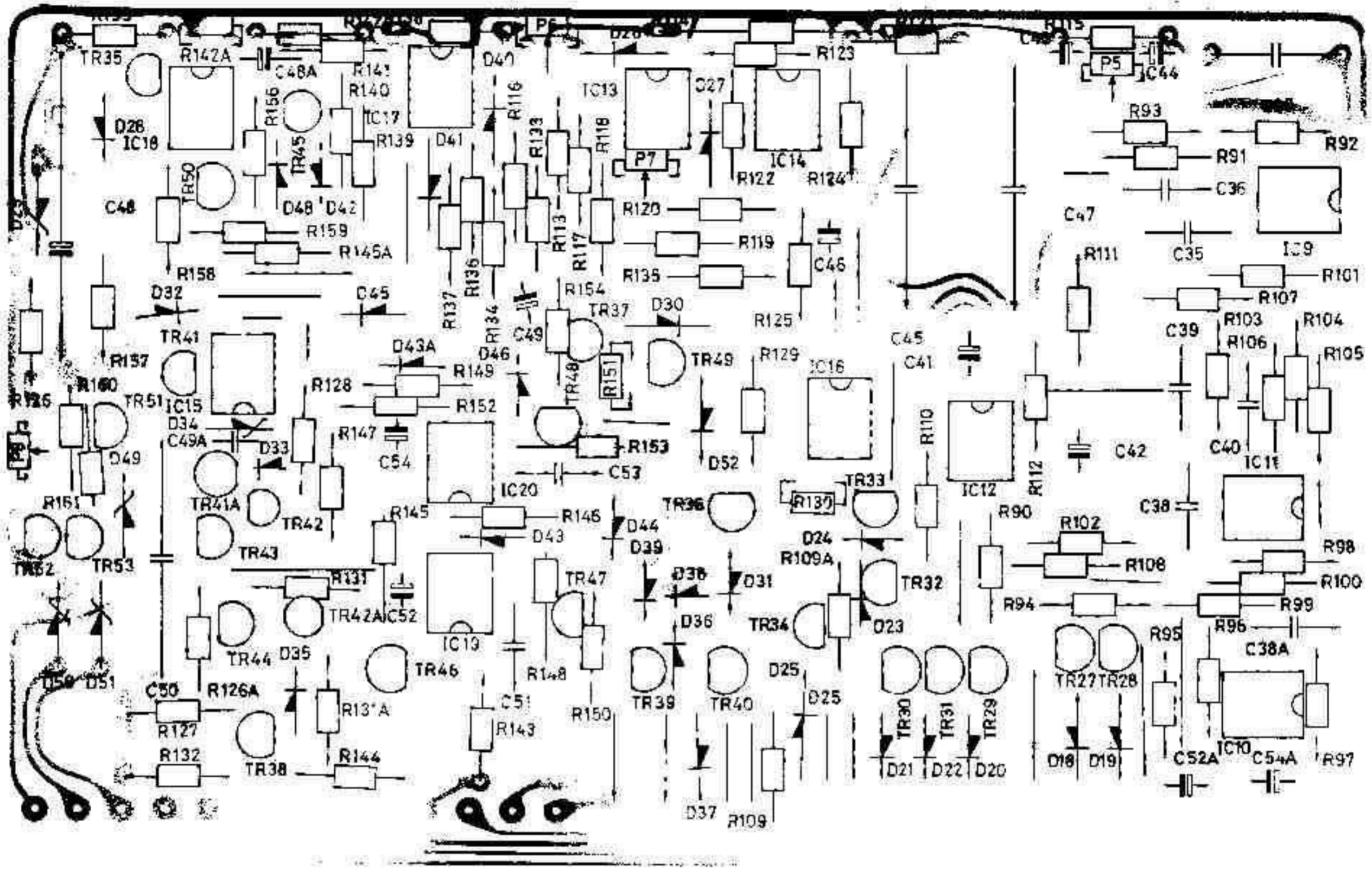


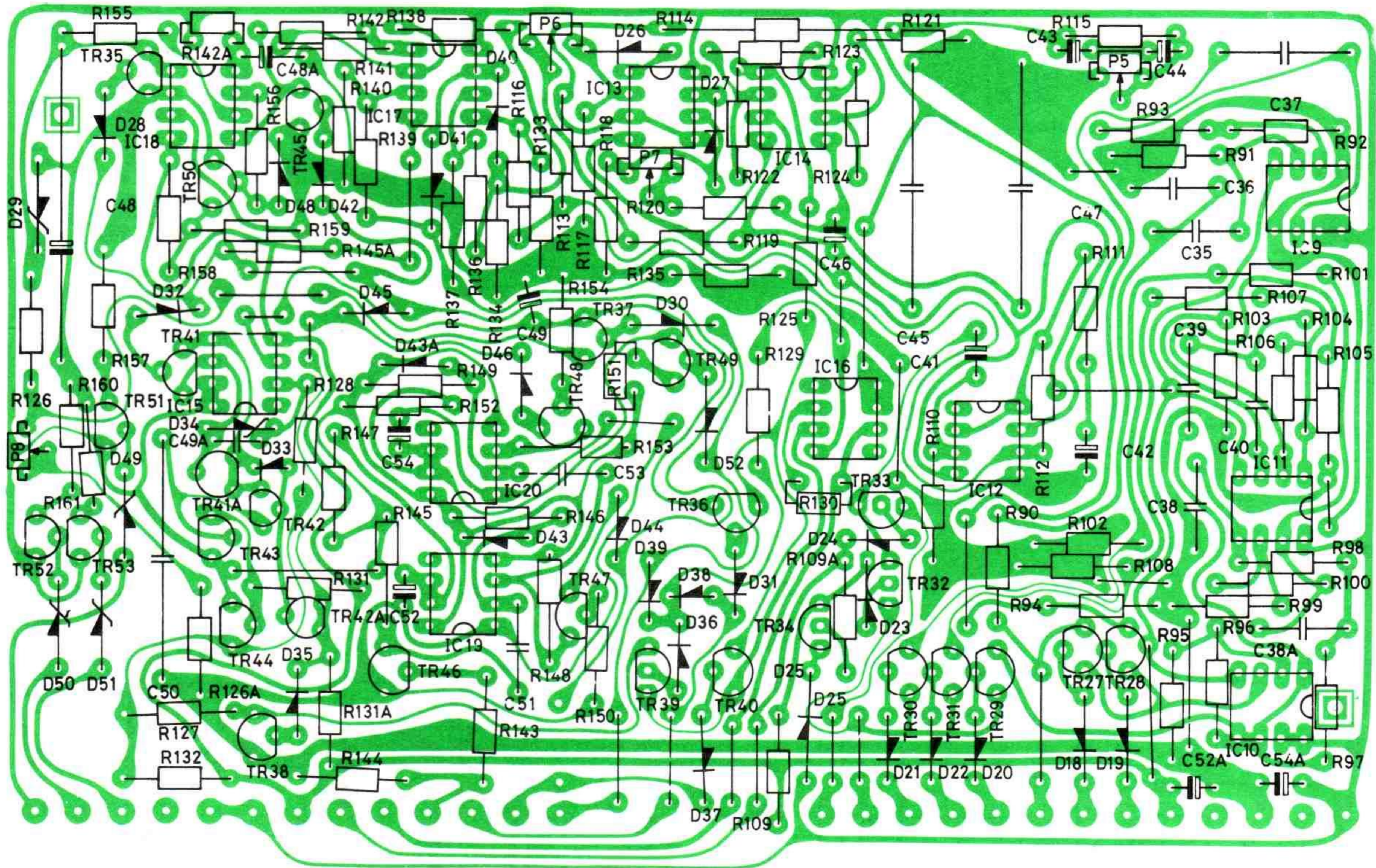
Diagram for circuit board B.  
Input stage, detector, attenuator etc.  
(TR1... TR26, IC1...IC8).

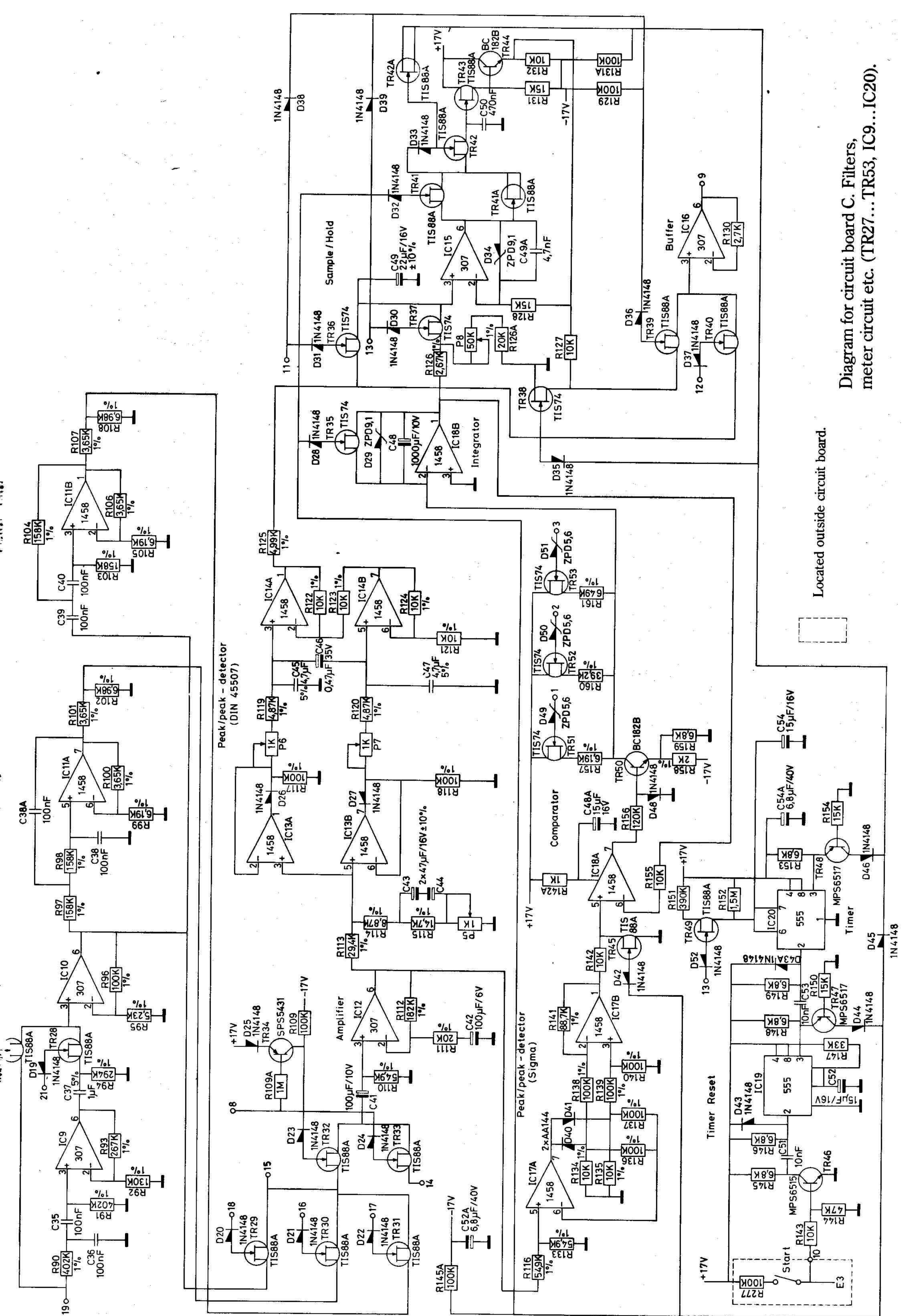
Located outside circuit board.



Parts layout for circuit board C.  
 Filters, meter circuit etc.  
 (TR27... TR53, IC9...IC20).



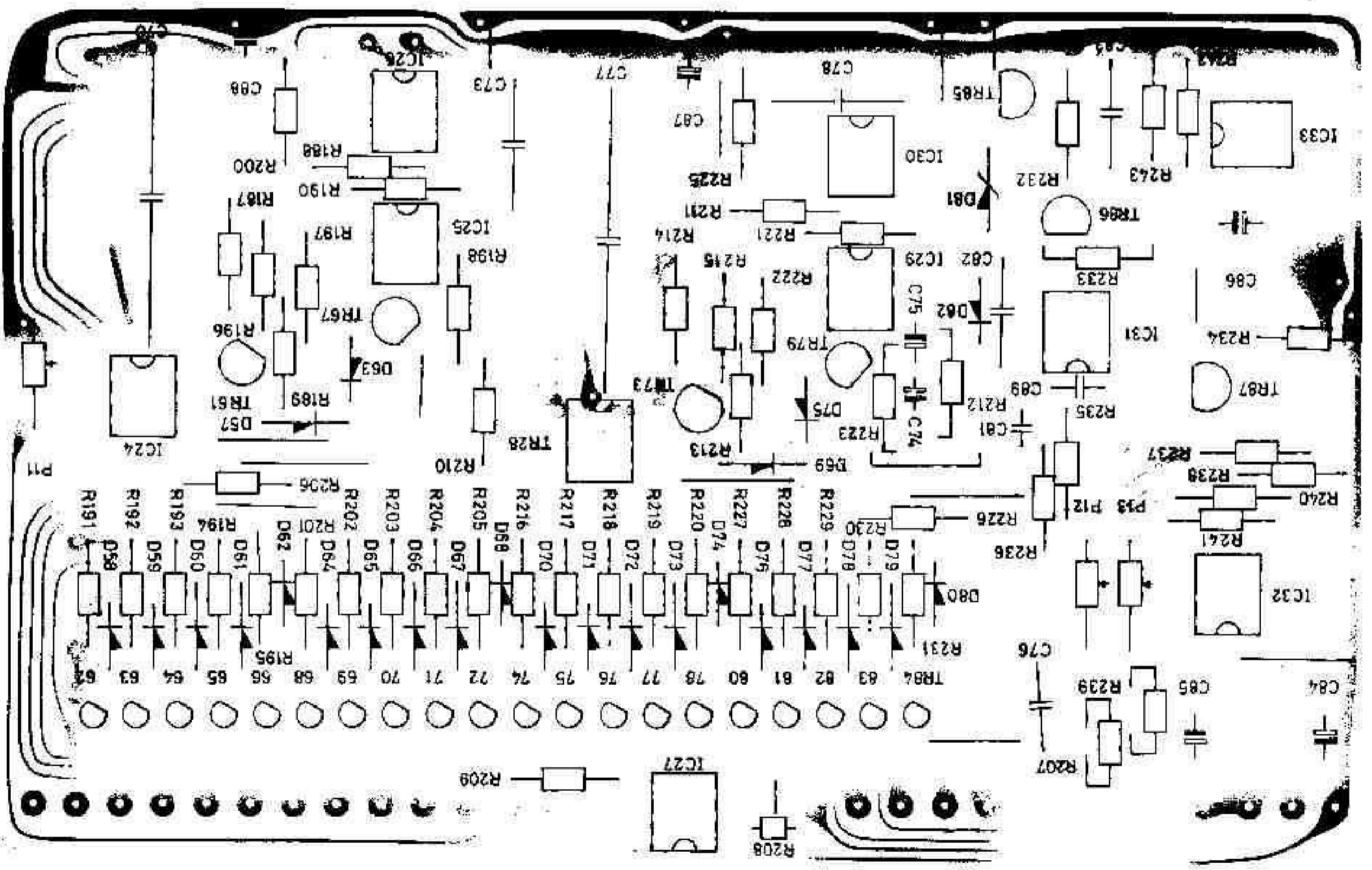


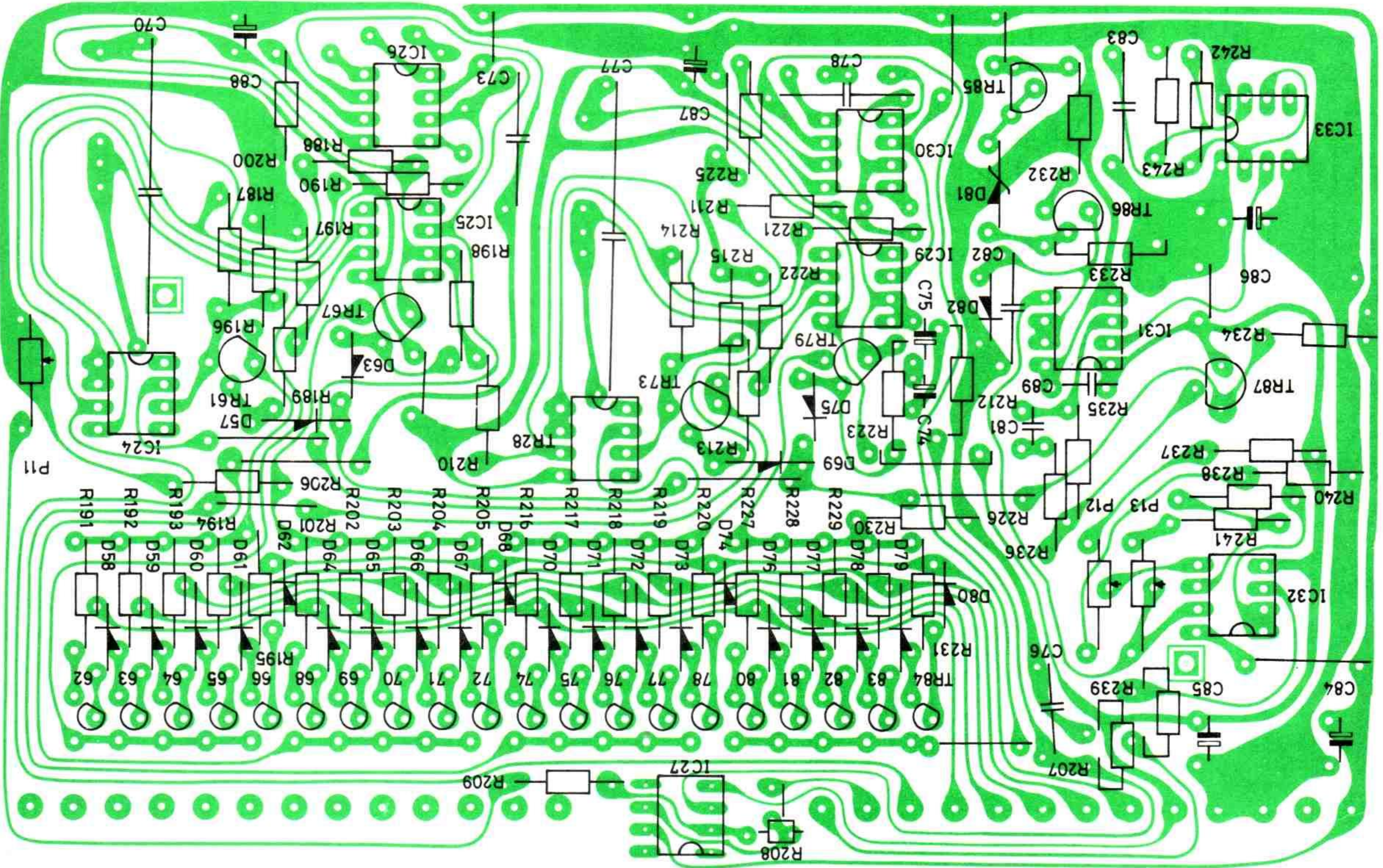


Located outside circuit board.

Diagram for circuit board C. Filters, meter circuit etc. (TR27...TR53, IC9...IC20).

Parts layout for circuit board D.  
Frequency analyser (TR61...TR87,  
IC24...IC33).





Variable Bandpass Filter

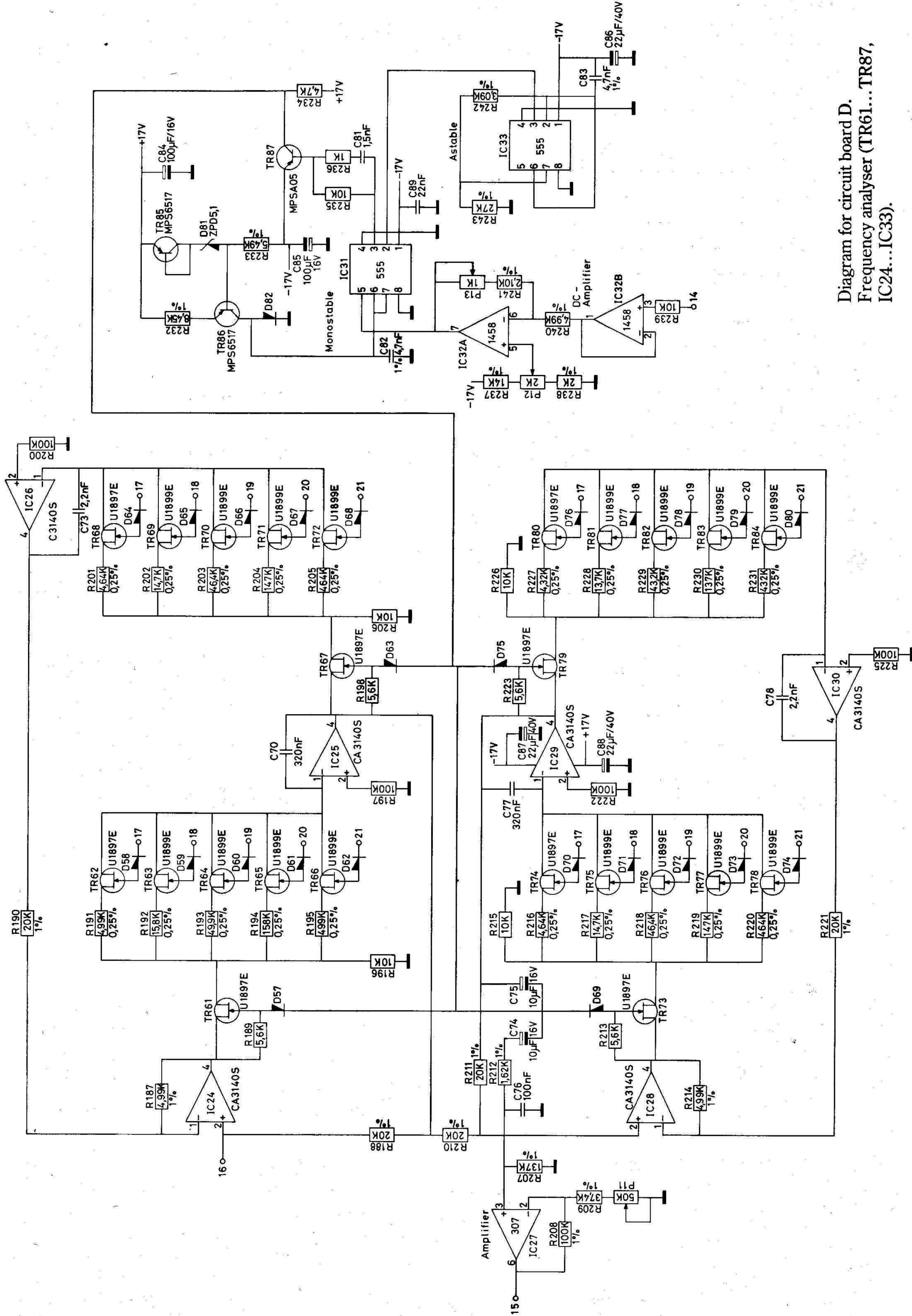
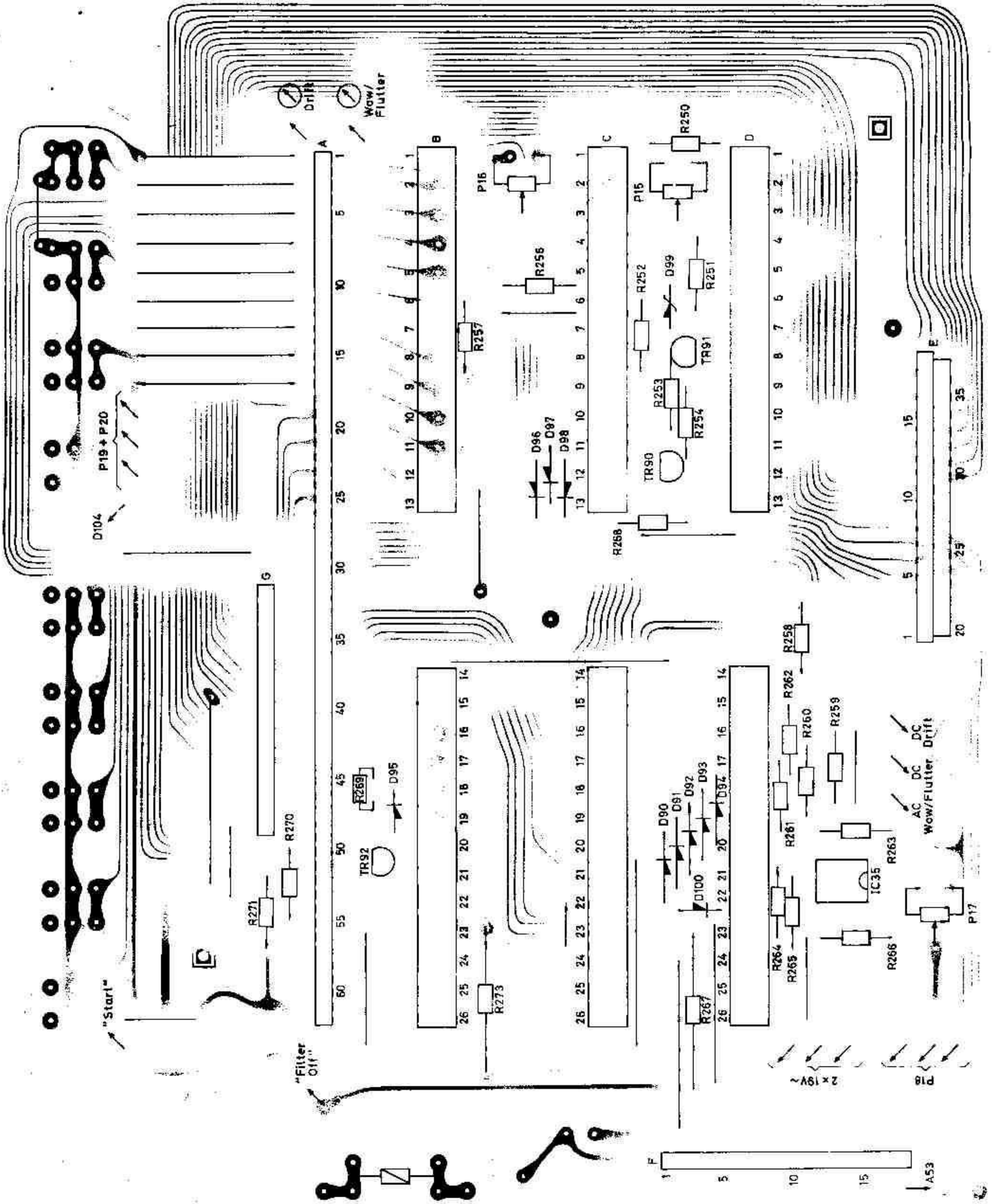
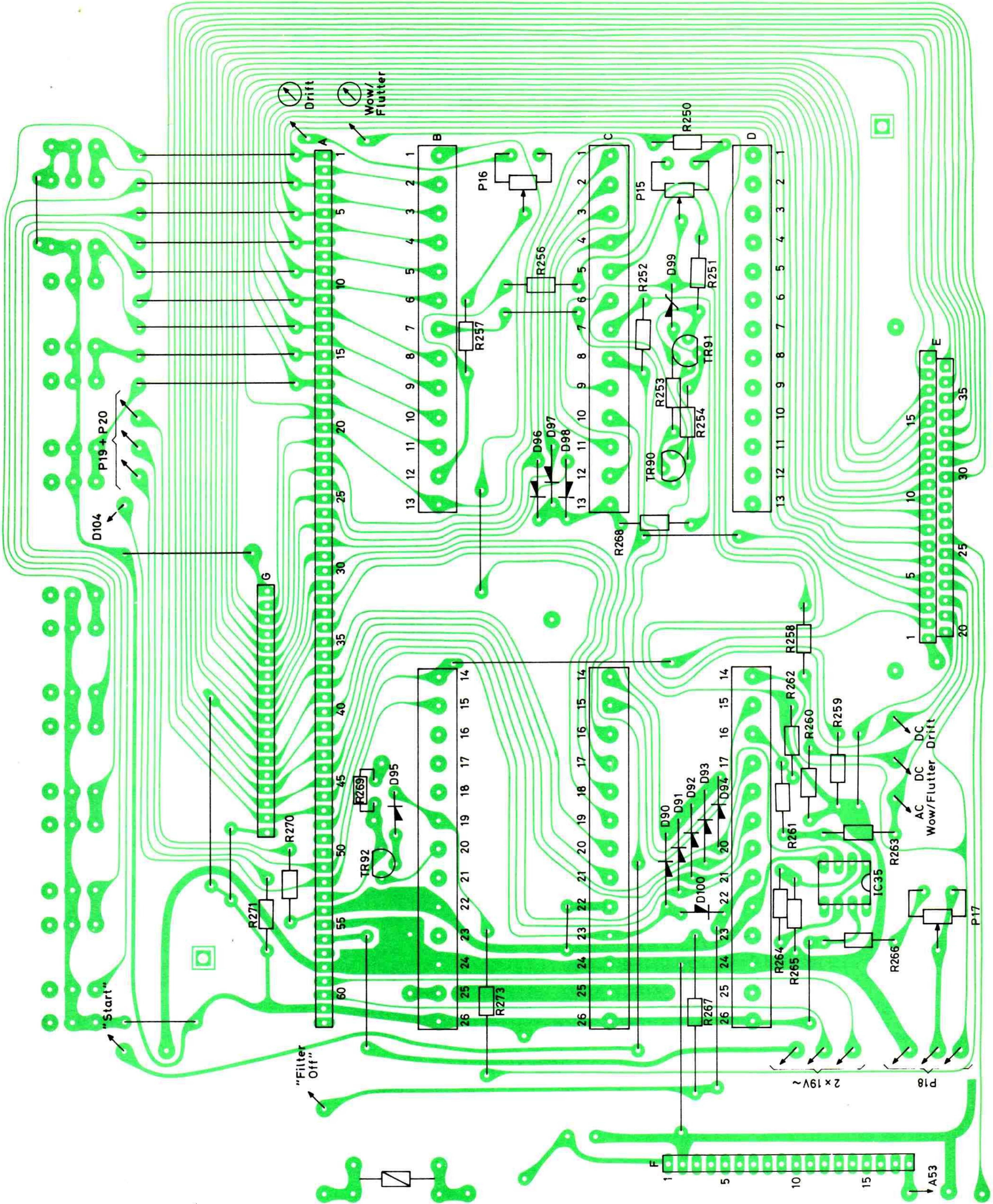
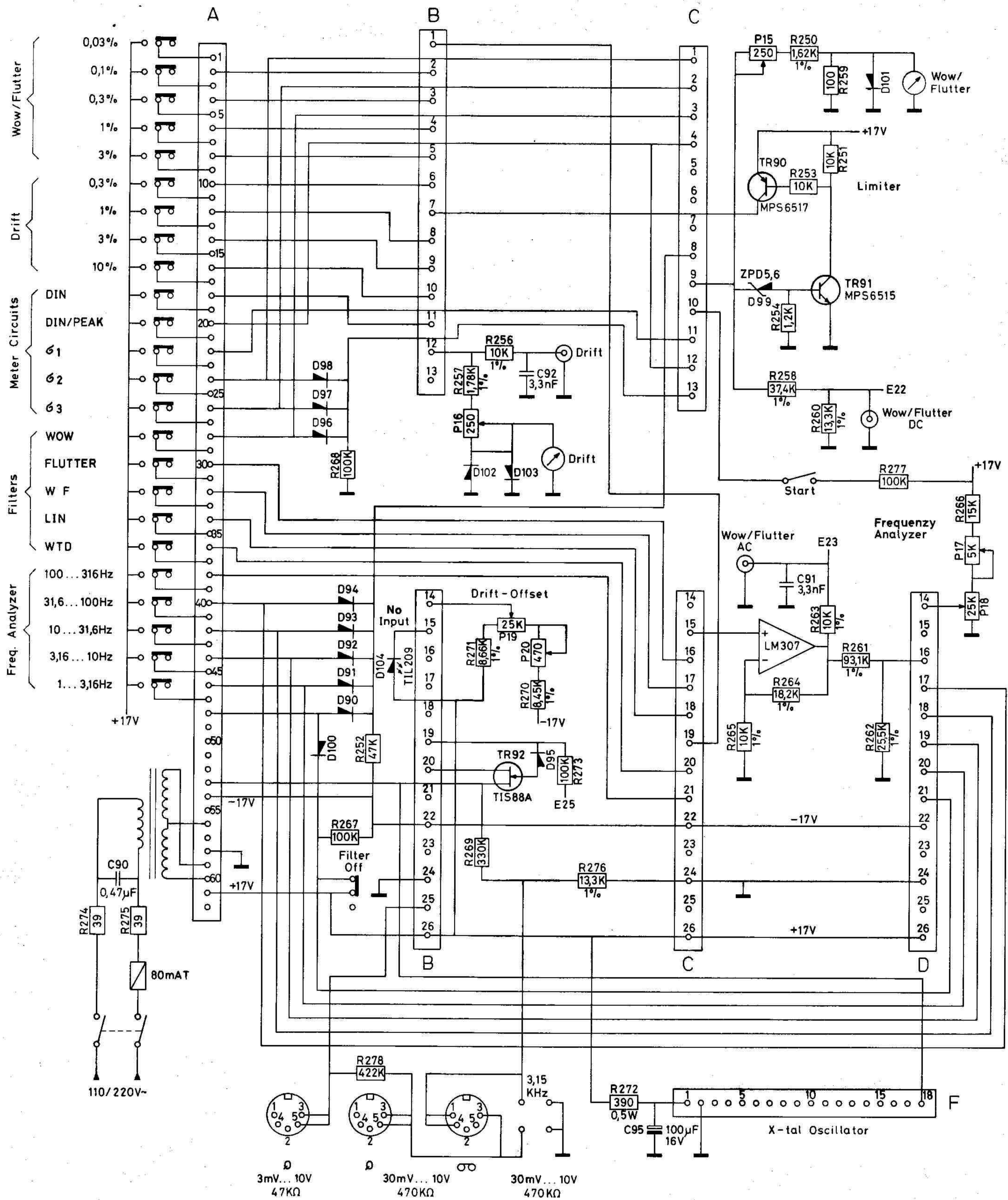


Diagram for circuit board D.  
Frequency analyser (TR61... TR87,  
IC24... IC33).



Parts layout for circuit board E.  
Bottom board. (TR90... TR92, IC35).





Diodes: 1N4148

Diagram for circuit board E.  
Bottom board. (TR90... TR92, IC35).